



ERPUG - European Road Profile User´s Group 2023
25 - 27 October - 10 years anniversary
Athens, Greece

New M-E Pavement design and performance prediction method

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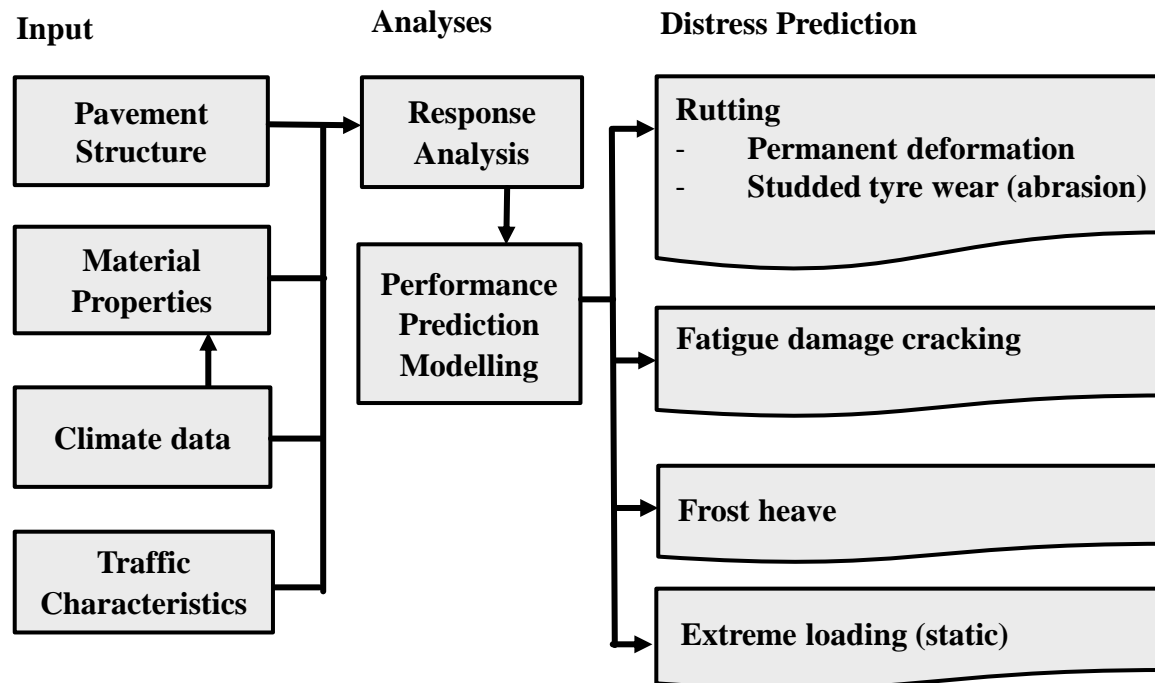
Linköping, Sweden

Overview

- ▶ **Overview of the M-E design tool ERAPave PP**
- ▶ **Input parameters**
 - Traffic, Climate, Material properties
- Response model**
- ▶ **Distress development (performance)**
 - Rutting
 - Fatigue cracking
 - Studded tyre wear (abrasion)
 - Frost heave
 - Bearing capacity control
- ▶ **Material databank**
- ▶ **Validation**
- ▶ **Further developments**
- ▶ **Summary**

ERAPave PP

ERAPave PP (Elastic Response Analysis of Pavements - Performance Prediction) is a **Mechanistic-Empirical** pavement analysis and design tool for **flexible** pavement. ERAPave PP predicts the evolution of **rutting**, **fatigue cracking** and **studded tyre wear** for a given pavement structure having a set of material properties. It further predicts the expected **frost heave** and controls the stability of a **extreme static loading** condition.



ERAPave PP

- ▶ The software can be downloaded from:
 - ▶ vti.se/en
 - ▶ Research
 - ▶ Highway engineering and maintenance
 - ▶ Pavement technology
 - ▶ Pavement design models for roads
- Version 0.93 is now available

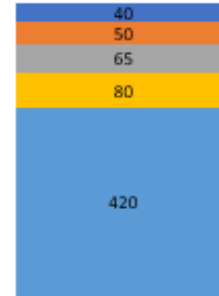
Output

Report

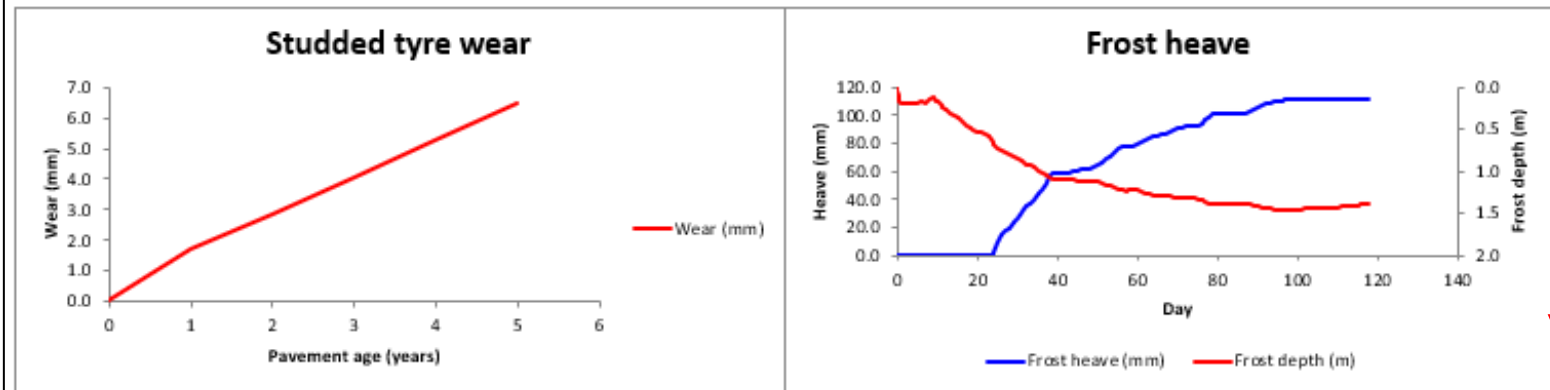
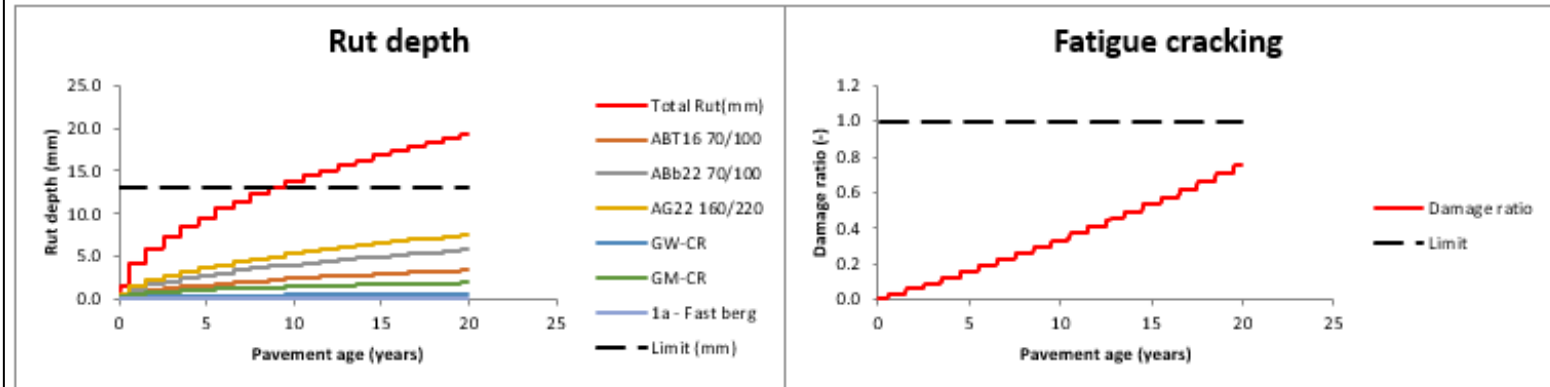
Summary

- Input data
- Predicted damages
 - rutting and wear
 - fatigue
 - Frost heave

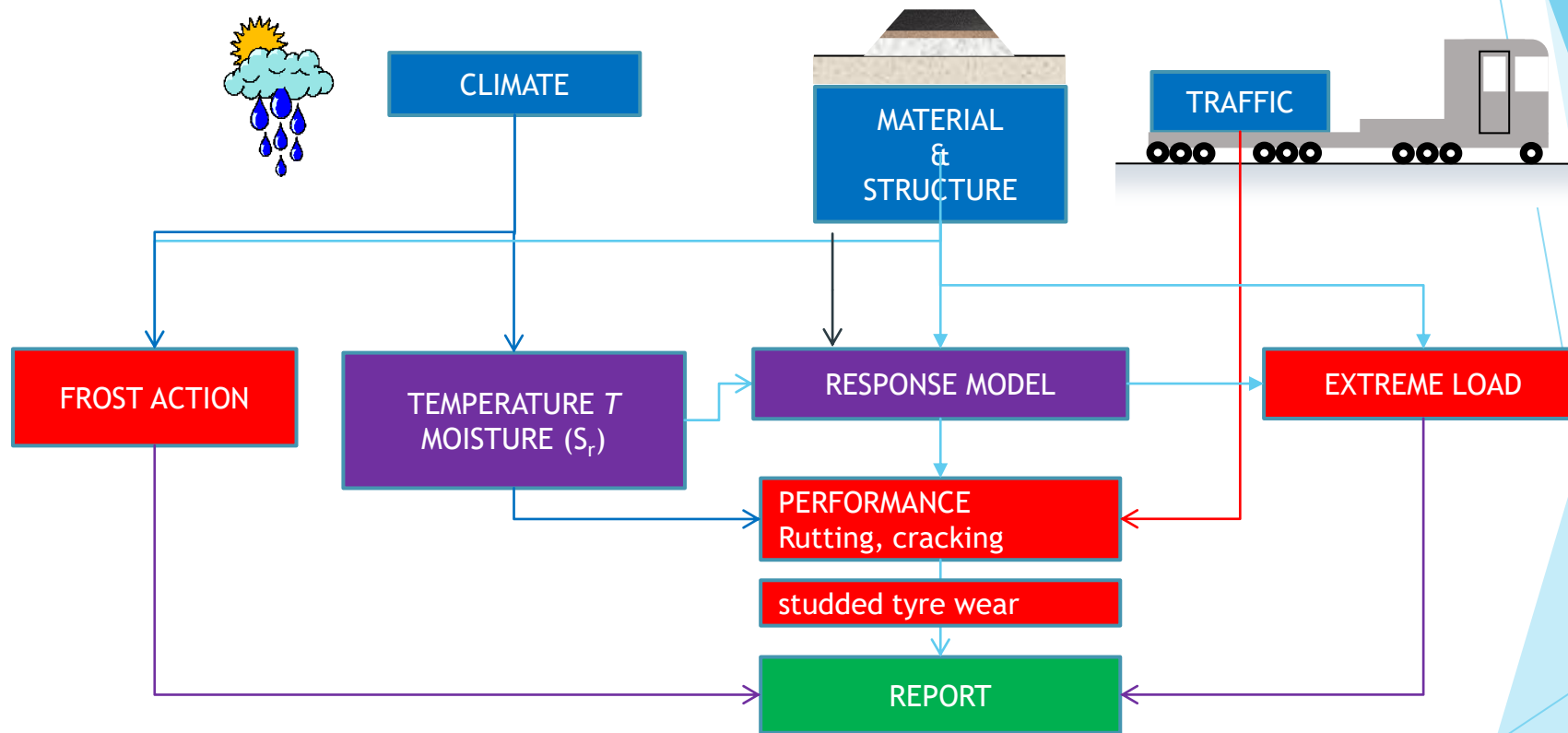
Road Section TEST
Date 2021-11-30



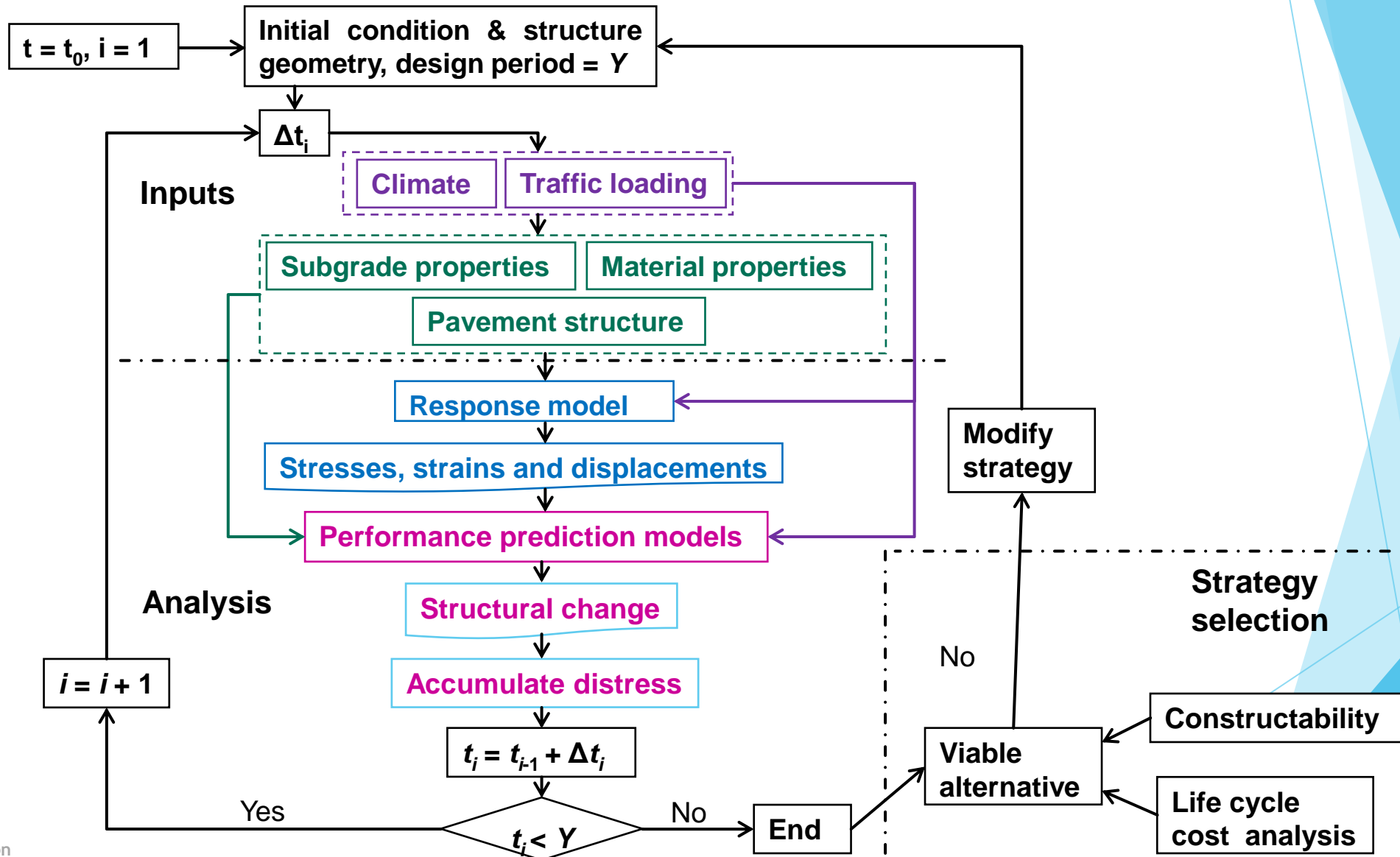
Layer	Rutting (mm)
ABT16 70/100	3.4
ABb22 70/100	5.8
AG22 160/220	7.6
GW-CR	0.7
GM-CR	1.9
1a - Fast berg	0.0
Total rutting	19.4
Studded tyre wear	6.4
Fatigue life	0.7
Frost heave	111.5
Frost depth	1.4



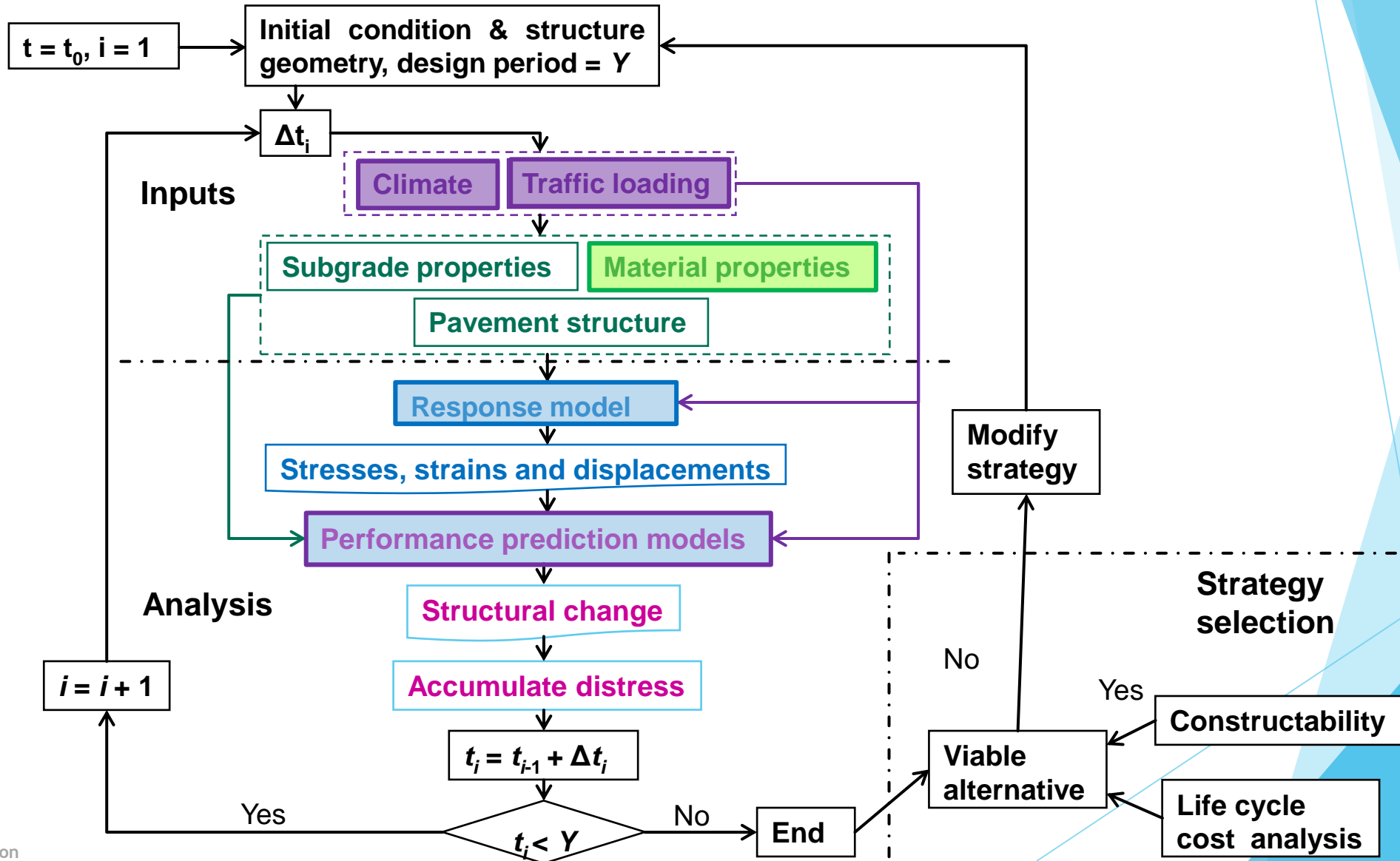
ERAPave PP components



Flexible pavement design - rutting and fatigue cracking



Flexible pavement design - rutting and fatigue cracking



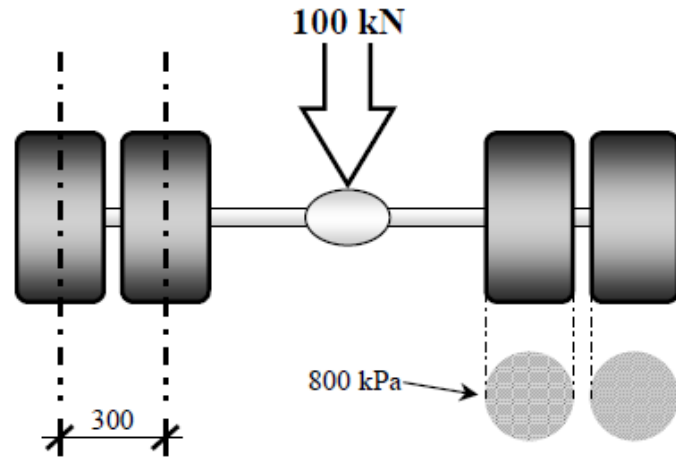
Traffic characteristics

- ▶ Traffic input is either:
 - ▶ Equivalent Single Axle Loads - ESAL 's
 - ▶ Axle Load Spectra - ALS from WIM-systems
- ▶ Lateral wander is included
- ▶ Traffic Growth factor is considered.



Traffic Loading: Standard axels

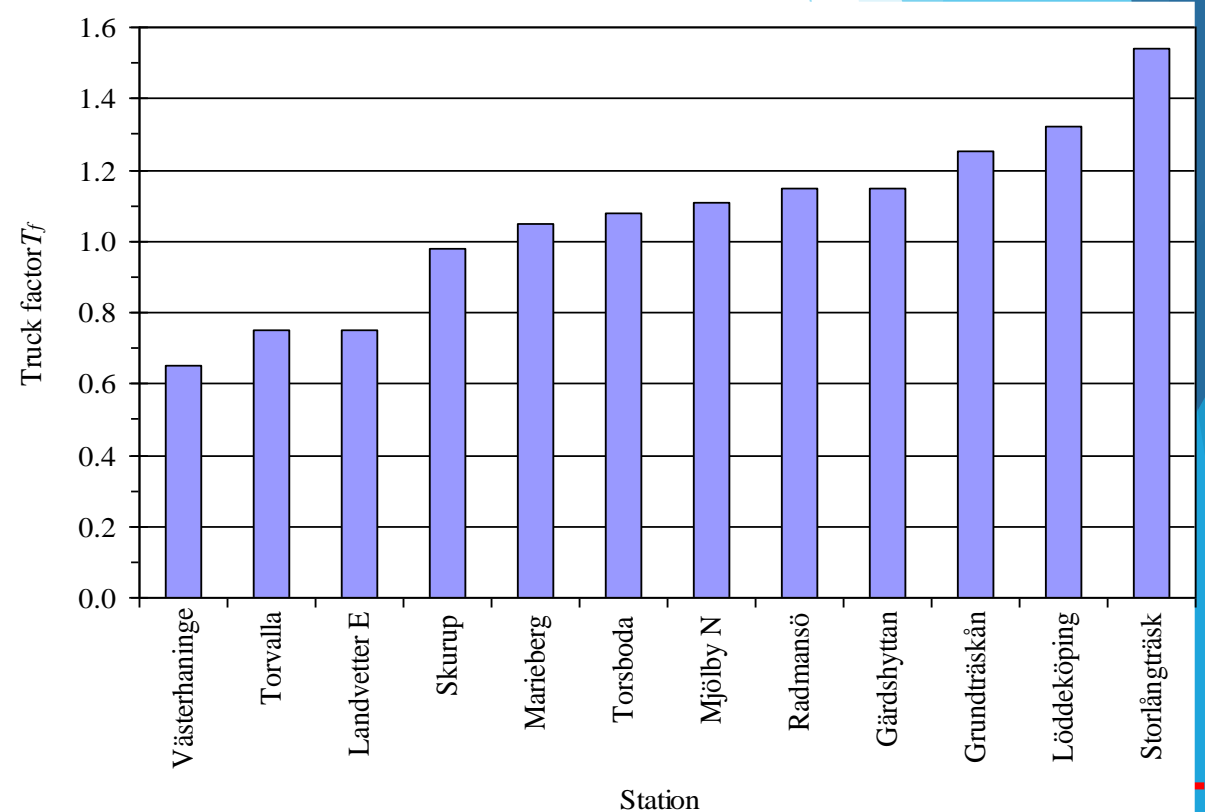
- ▶ Standard axels - Dual tyre configuration $W = 100$ kN, $p = 800$ kPa, c/c 300 mm



$$N_{ekv} = AADT_l \cdot 3.65 \cdot S_h \cdot T_f \cdot \sum_{j=1}^n \left(1 + \frac{k}{100} \right)^j$$

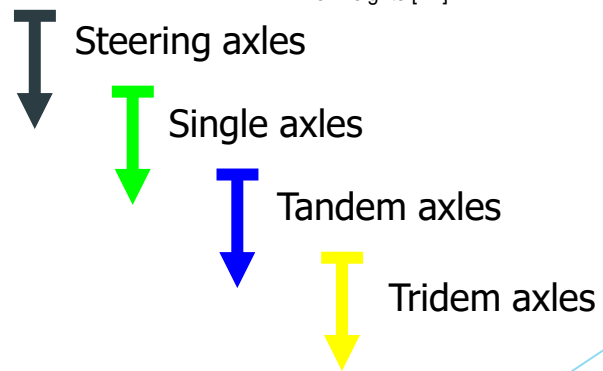
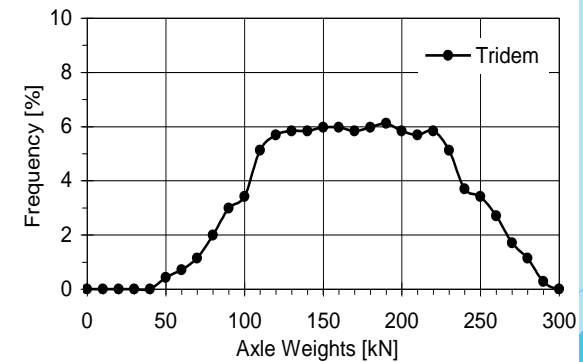
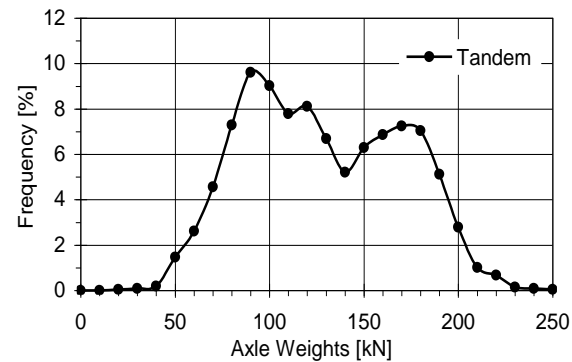
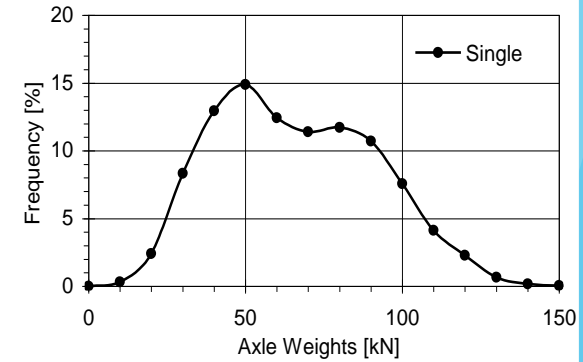
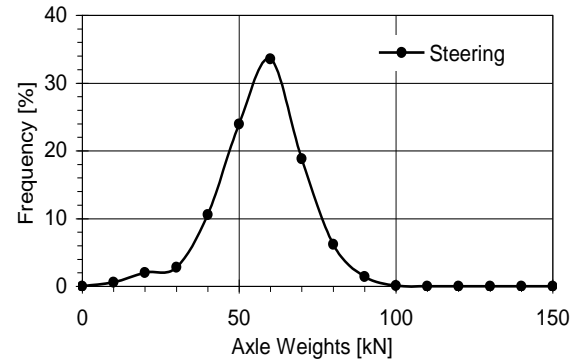
$$T_f = \frac{1}{N_{hv}} \cdot \sum_{i=1}^4 N_i \cdot \sum_{j=1}^{n_j} \left(\frac{W_{ij}}{W_{i_{stand}}} \right)^4 \cdot \frac{f_j^{norm}}{100}$$

Truck factor based on 12 WIM locations.

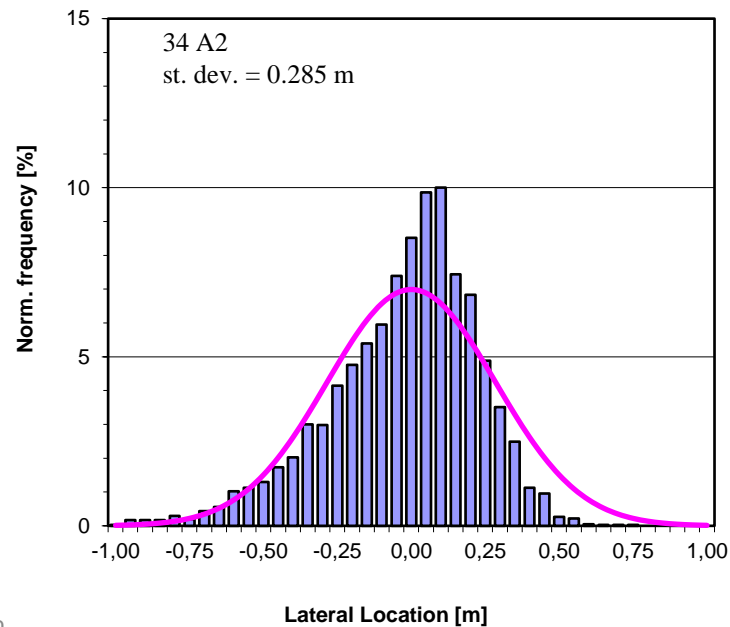
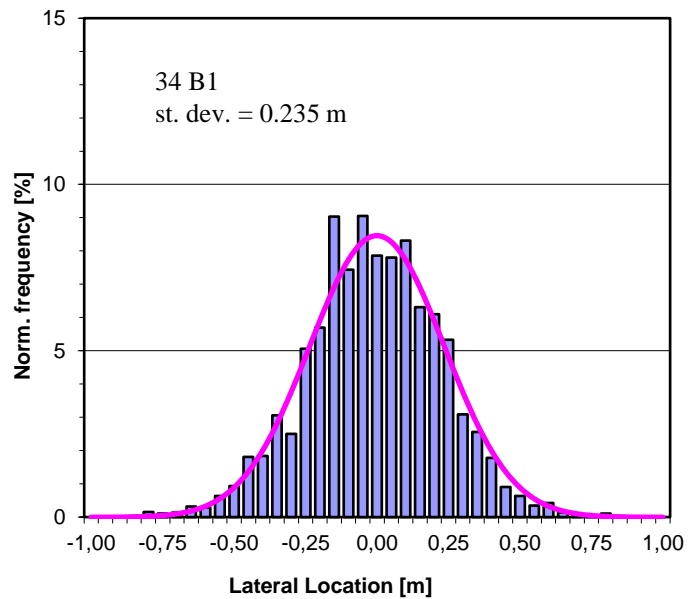
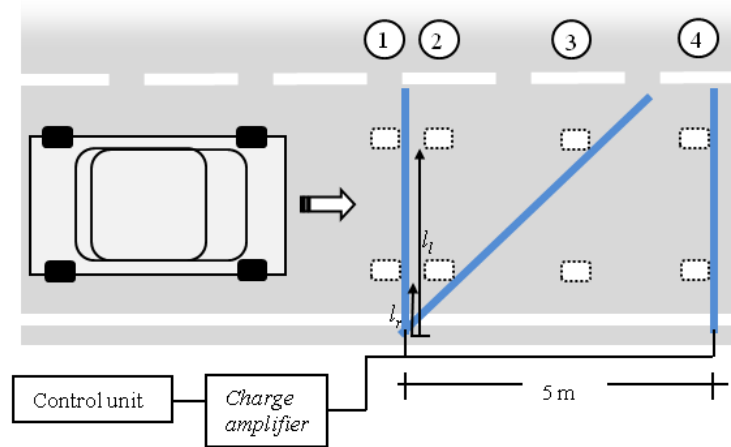
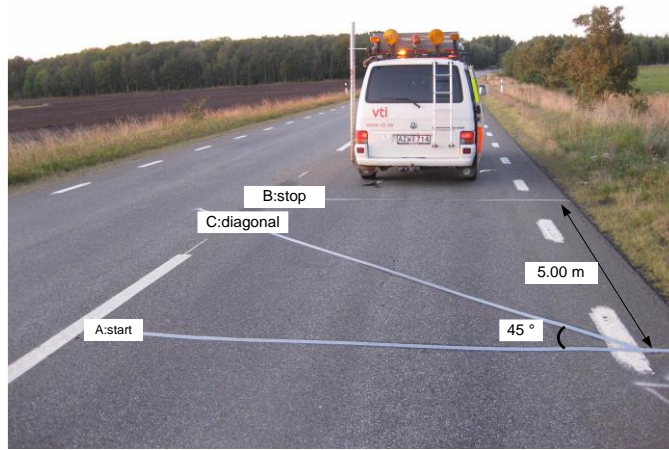


Traffic loading: Axle Load Spectra (ALS)

Weigh-In-Motion (WIM) data



Traffic Loading: Lateral Wander



Climate dependency

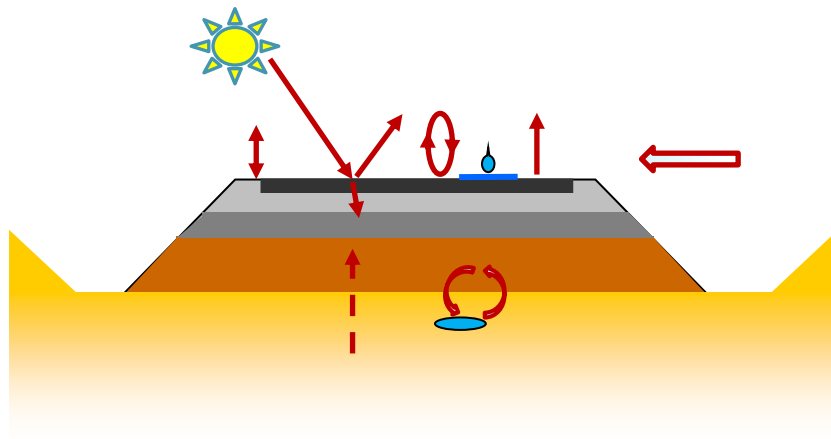


Climate dependency

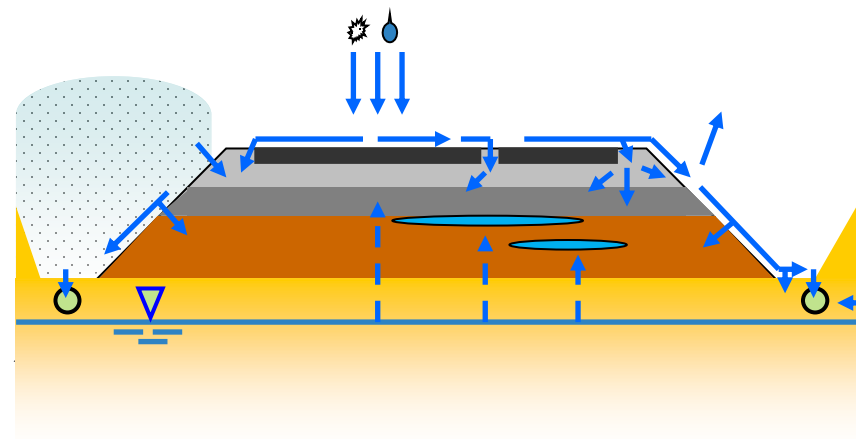
Pavement response and degradation is highly dependent on the climate variables.

The two most important variables are **temperature T** and **moisture content w** (or degree of saturation S_r).

Heat balance

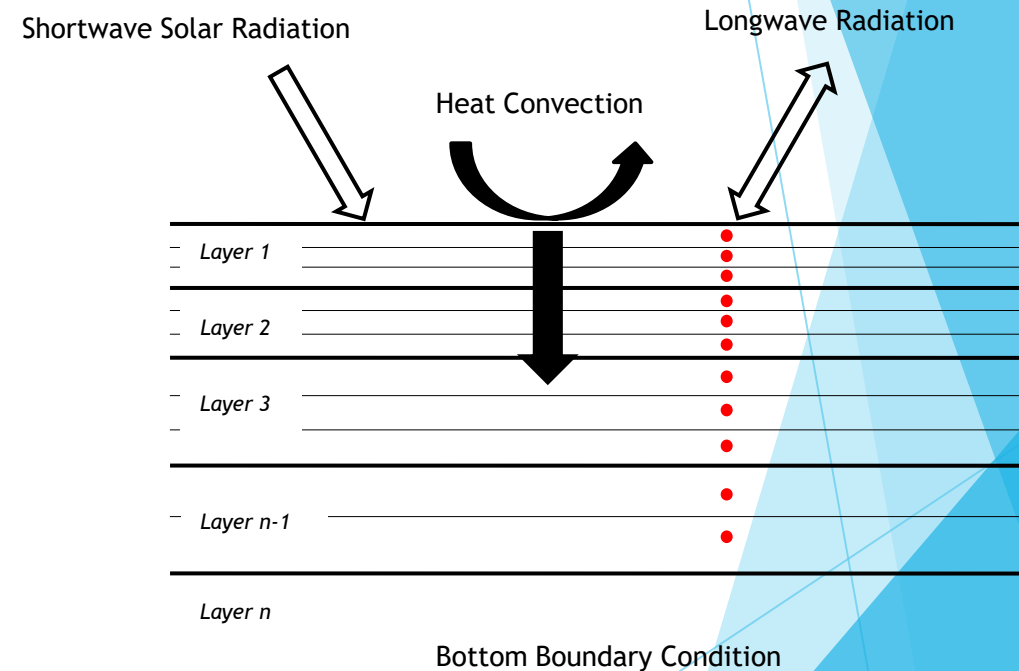


Water balance



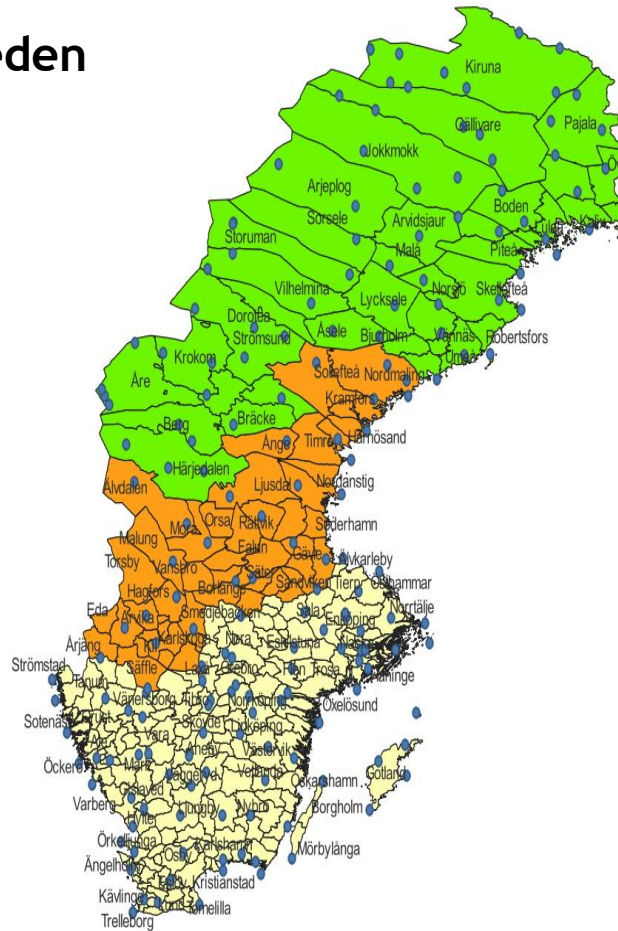
Heat balance: Temperature model

- 1-D Finite control volume method (FCVM)
- A numerical approach for solving the heat equation
- Discretization into small control volumes
- Input for analysis
 - Air temperature
 - Wind speed
 - Solar radiation

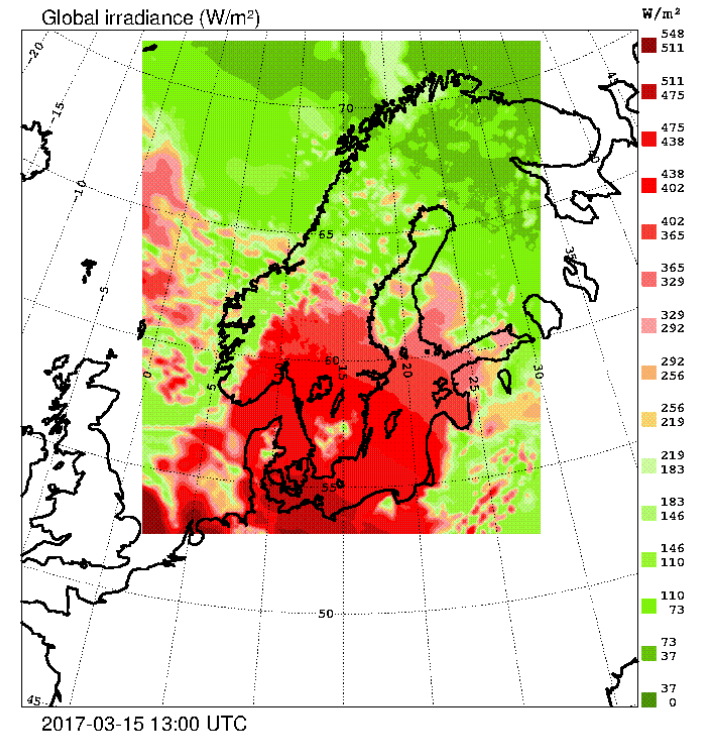
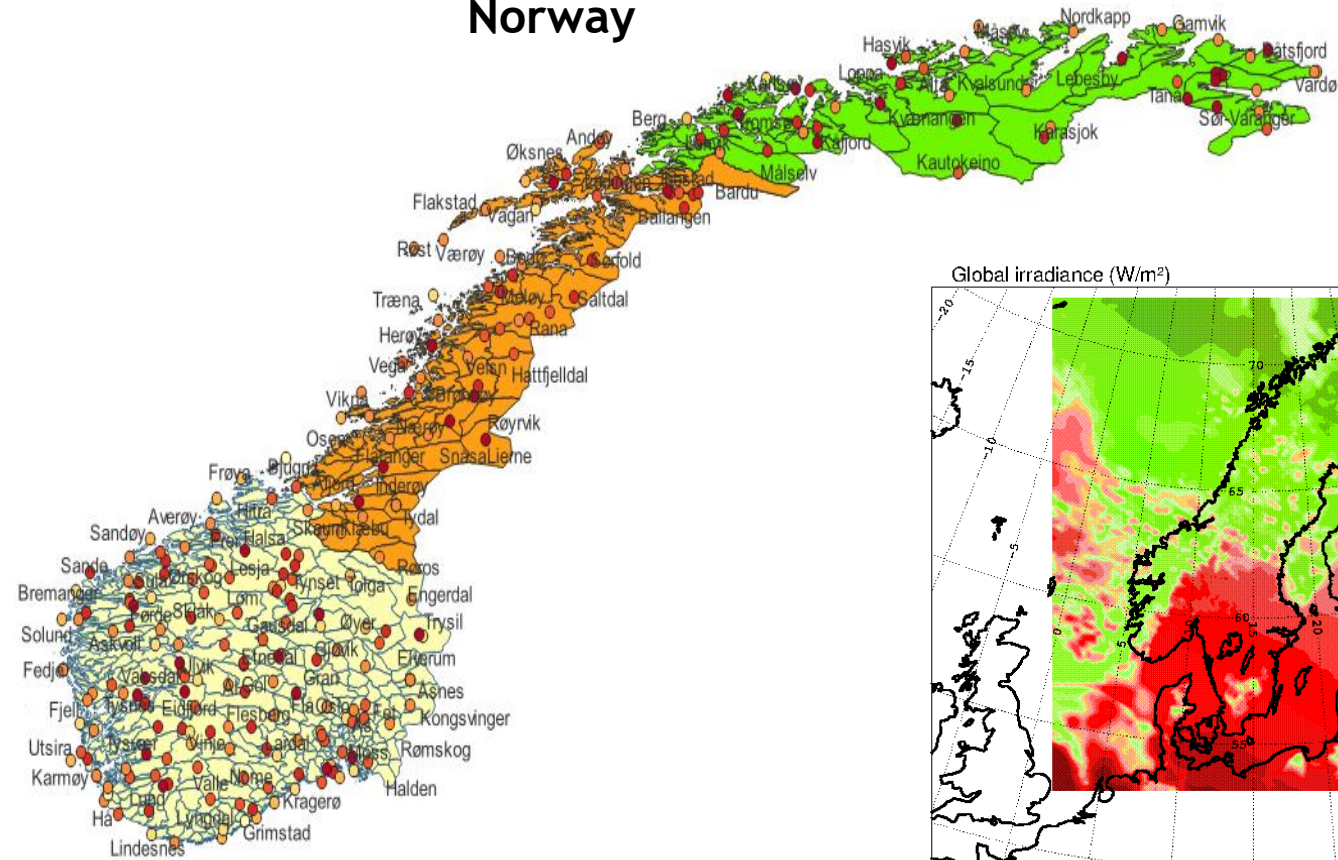


Climate data - Smhi.se and Frost.MET.no API

Sweden



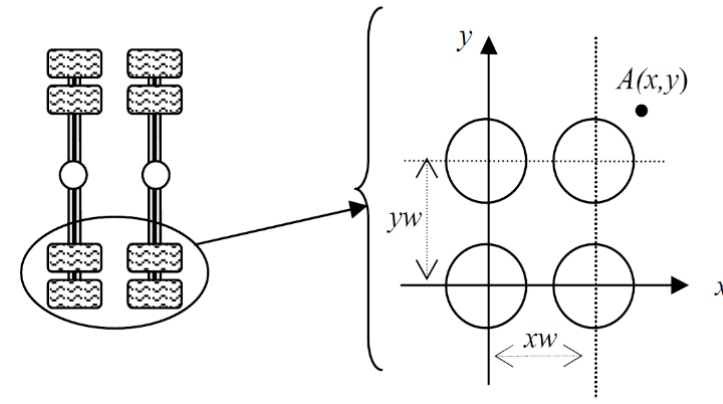
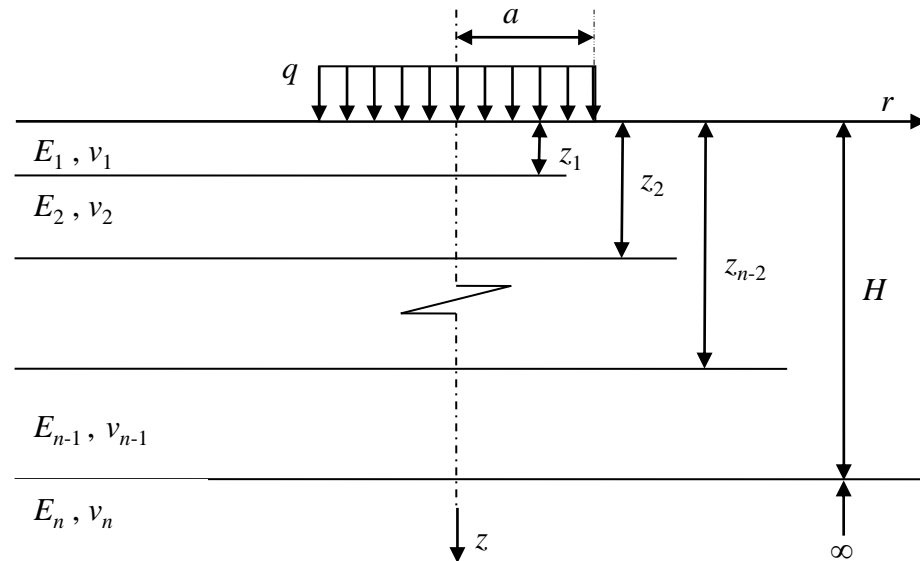
Norway



Response model

MLET - Multi-layer elastic theory

The elastic response of the tyre pavement interaction is estimated by a linear/nonlinear MLET (multi layer elastic theory) approach giving the stresses and strains at desired locations.



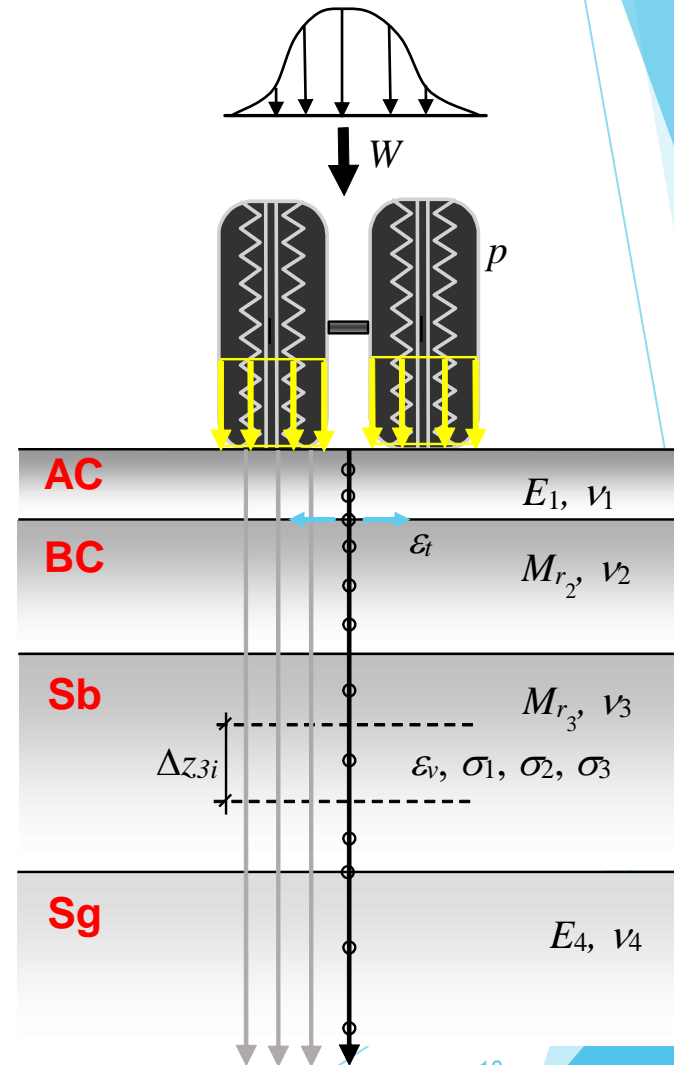
Response modelling

Based the MLET (MultiLayer Elastic Theory).

AC is temp. dependent - lin. elastic matr.

UGM:s are lin. or non-lin. (stress dependent) elastic material.

Lateral Wander is assumed normal distributed.



Response calculations

Stiffness of asphalt bound layers - Temperature dependency

Two models are included in ERAPave PP.

Sigmoidal model (master curve estimations)

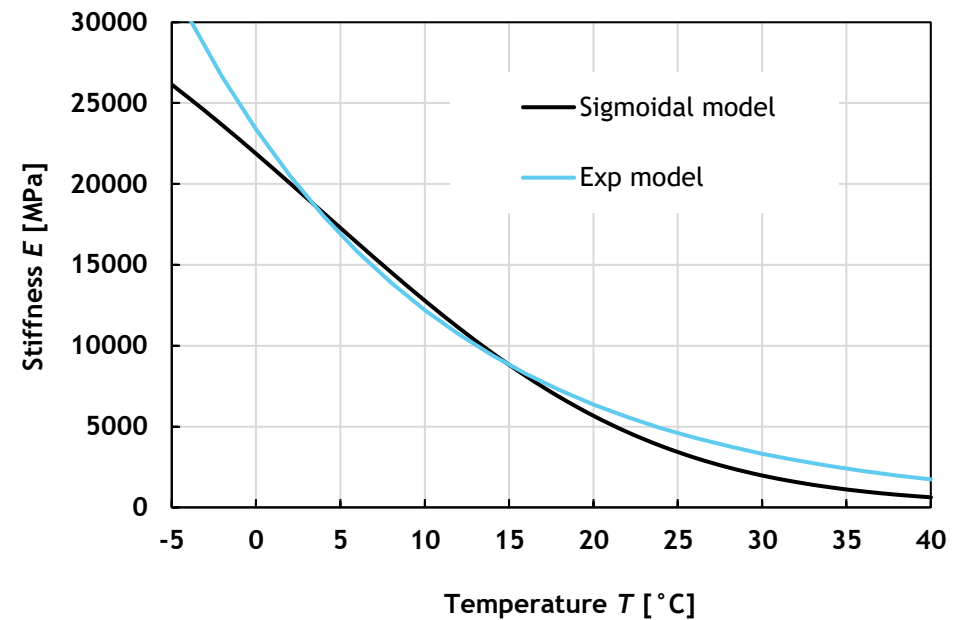
$$\log |E| = a + \frac{b}{1 + e^{(c-d \log f_r)}}$$

a , b , c and d are material parameters and f_r is reduced frequency linked to the vehicle speed and thickness of the HMA layer.

Exponential model

$$E = E_{ref} e^{-b(T-T_{ref})}$$

b is material parameter and E_{ref} is the stiffness at reference temperature T_{ref} .



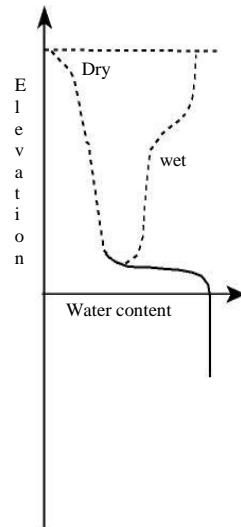
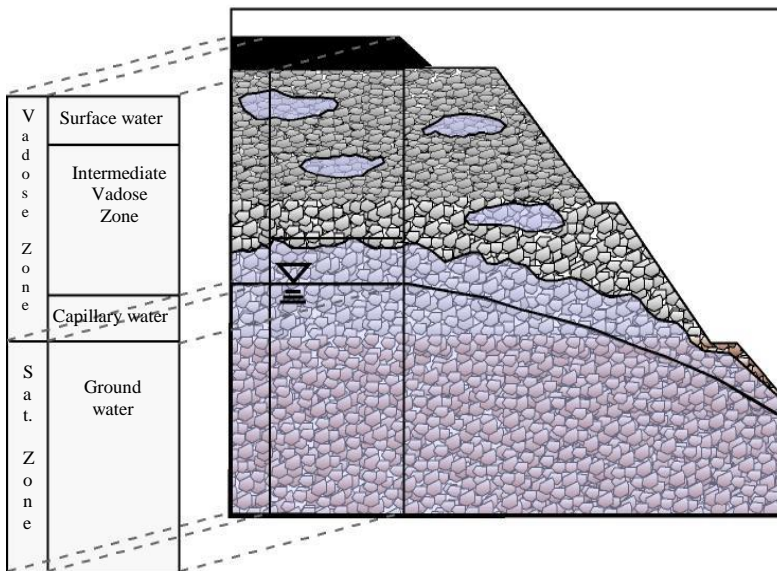
Response calculations

Stiffness of unbound layers and subgrades - Moisture dependency

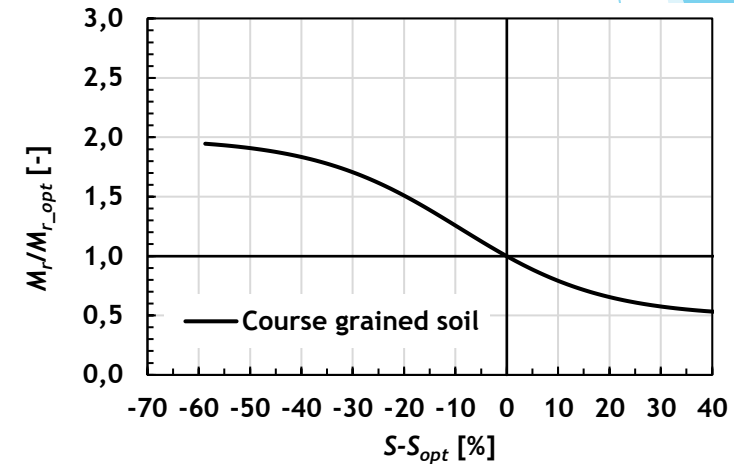
Stiffness - moisture content (degree of saturation) relationship is given as:

$$\log \frac{M_R}{M_{R_{opt}}} = a + \frac{b-a}{1 + \exp\left(\ln \frac{-b}{a} + k_m (S - S_{opt})\right)}$$

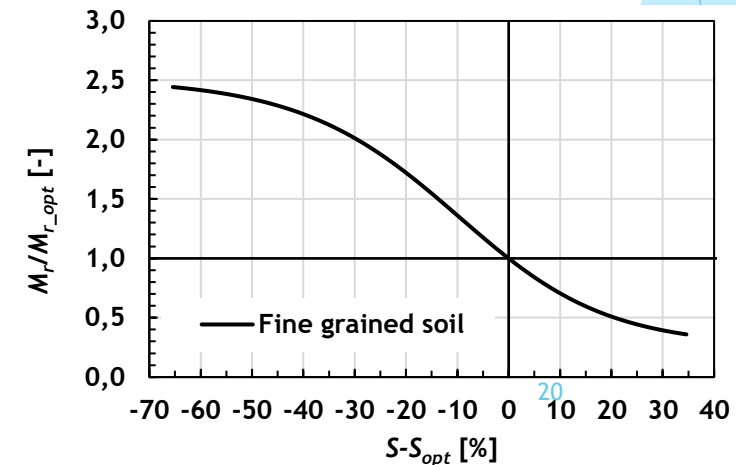
a , b and k_m are material parameters.



Base course and subbase matr.



Fine grained subgrade matr.



Performance prediction

- Fatigue cracking (bottom-up)
- Rutting (permanent deformation)
- Abrasion (studded tyre wear)
- Frost heave

Rutting (plastic deform.)



Fatigue cracking (bottom-up)



Abrasion (studded tyre wear)



Frost actions & frost heave damage



Performance predictions

Bottom-up fatigue cracking

Fatigue law: $N_f = a \varepsilon_{bt}^{-b} E^{-c}$ ($N_f = a \varepsilon_{bt}^{-b}$)

$$\log(N_f) = f_1 - f_2 \log \varepsilon_{bt} - f_3 E$$

Lab to field: $a_{field} = S a_{lab}$

► Miner's rule used for summation:

$$D = \frac{\sum n_i}{\sum N_{f_i}} \quad 0 \leq D \leq 1$$

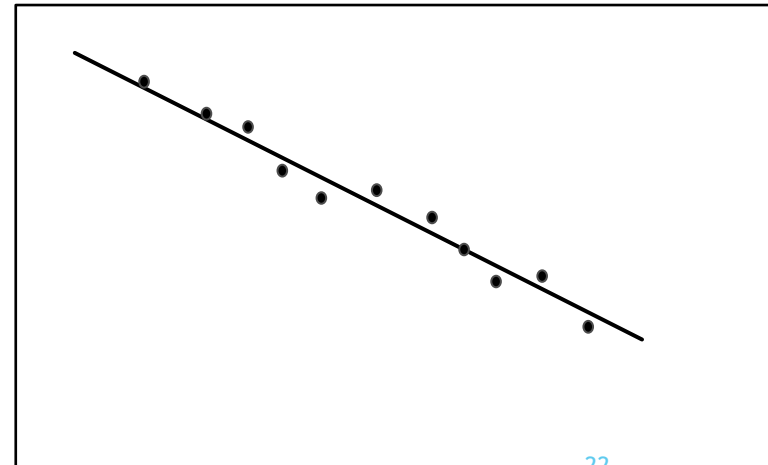
Typical input parameters:

$$f_1 = 14 \quad (12 - 15)$$

$$f_2 = b = 4 \quad (3 - 5)$$

$$f_3 = c = 0$$

$\log \varepsilon_{bt}$



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$\log(N_f)$

Performance predictions

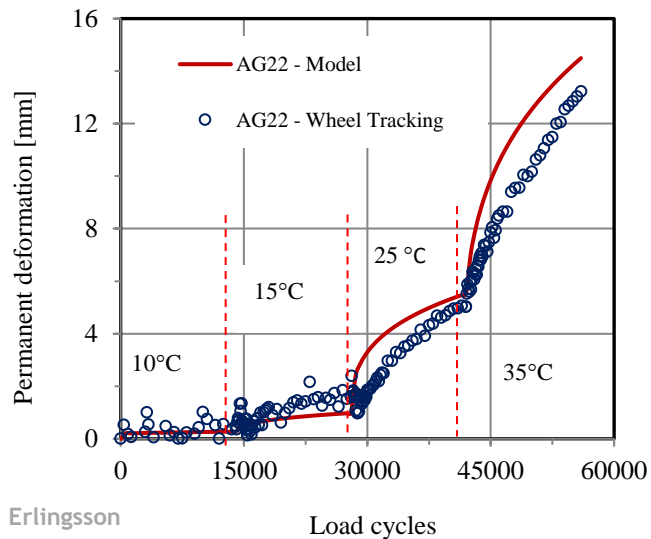
Plastic deformation (rut)

▶ AC: $\hat{\epsilon}_p(N) = a_1 T^{a_2} N^{a_3} \Delta \epsilon_r$ $\Delta \epsilon_r = \Delta \epsilon_r(T)$

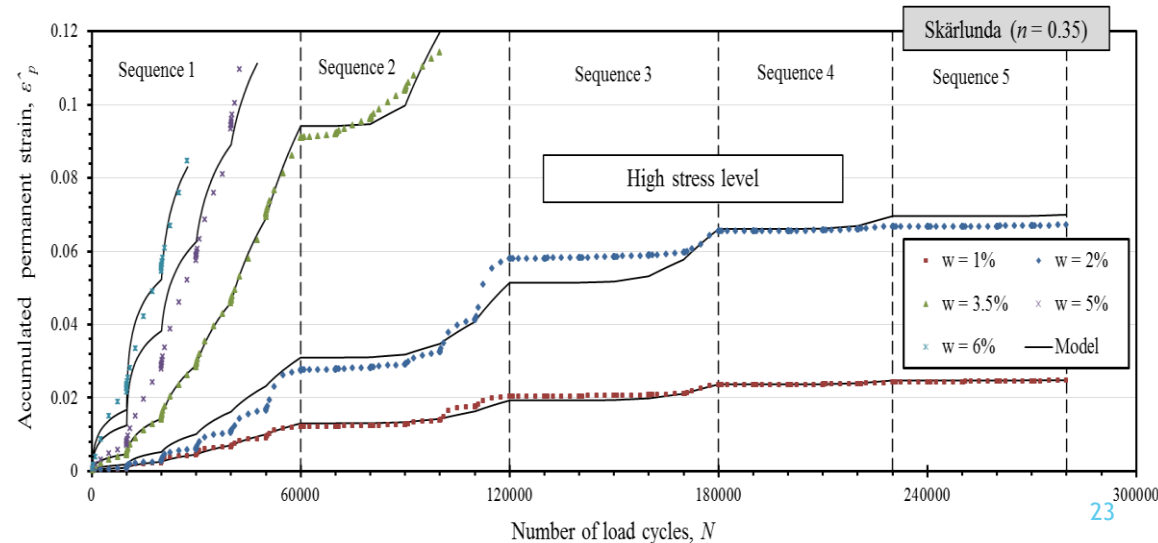
▶ UGM & soils: $\hat{\epsilon}_p(N) = a N^{b \Delta \epsilon_r} \Delta \epsilon_r = (c_1 + c_2 S_r) N^{b \Delta \epsilon_r} \Delta \epsilon_r$ $\Delta \epsilon_r = \Delta \epsilon_r(S_r)$

$$\hat{\epsilon}_p(N) = \left(\frac{\epsilon_0}{\Delta \epsilon_r^{ref}} \right) e^{\left(\frac{\rho}{N} \right)^\beta} \Delta \epsilon_r$$

AC layers

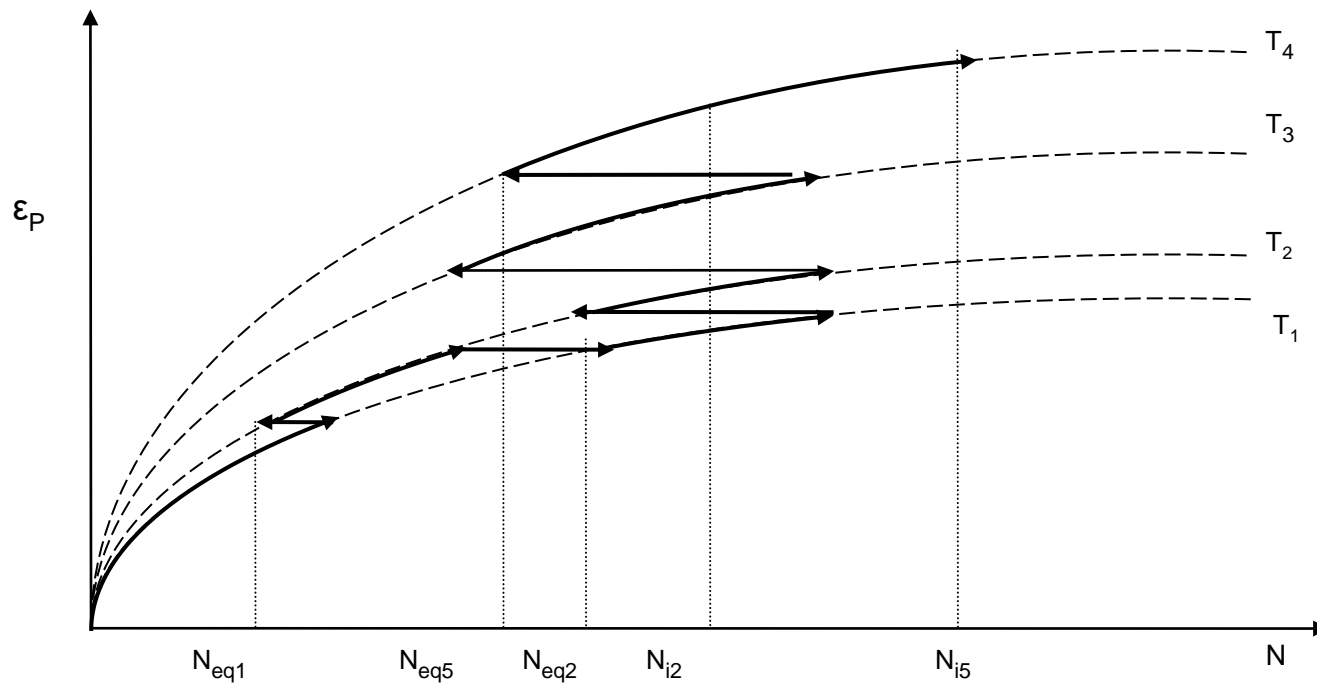


Unbound layers



Accumulation (Superposition) of perm. strain

Time hardening approach



Step j

$$N_{eq_j} = \left[\frac{\hat{\varepsilon}_{p_{j-1}}}{\hat{\varepsilon}_{p_j}(N=1)} \right]^{\frac{1}{m}}$$

$$\hat{\varepsilon}_{p_j} = \hat{\varepsilon}_{p_{j-1}} + \hat{\varepsilon}_{p_j}(N=1) \cdot \left[(N_{eq_j} + \Delta N)^m - N_{eq_j}^m \right]$$

$j = j+1$

Next j

Studded tyre abrasion

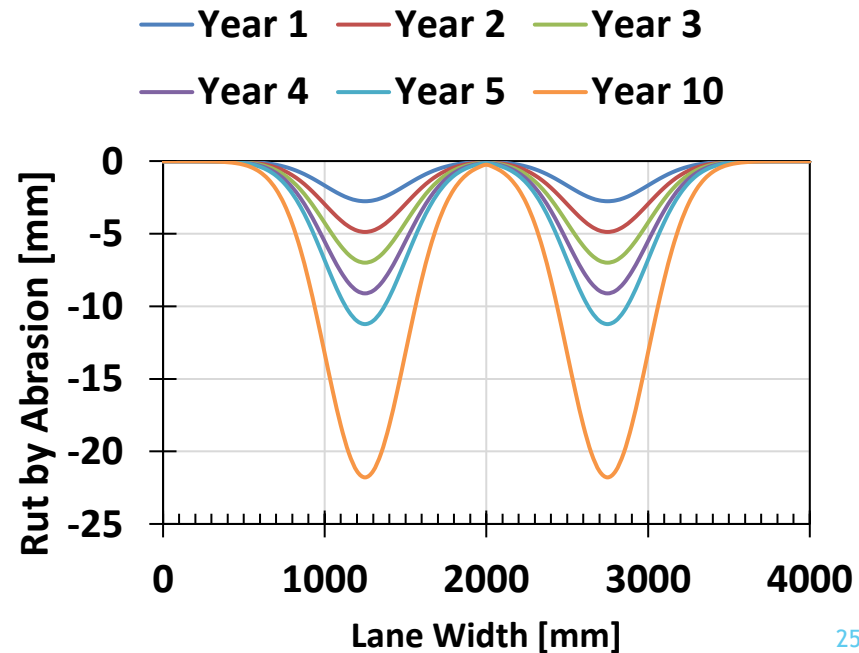
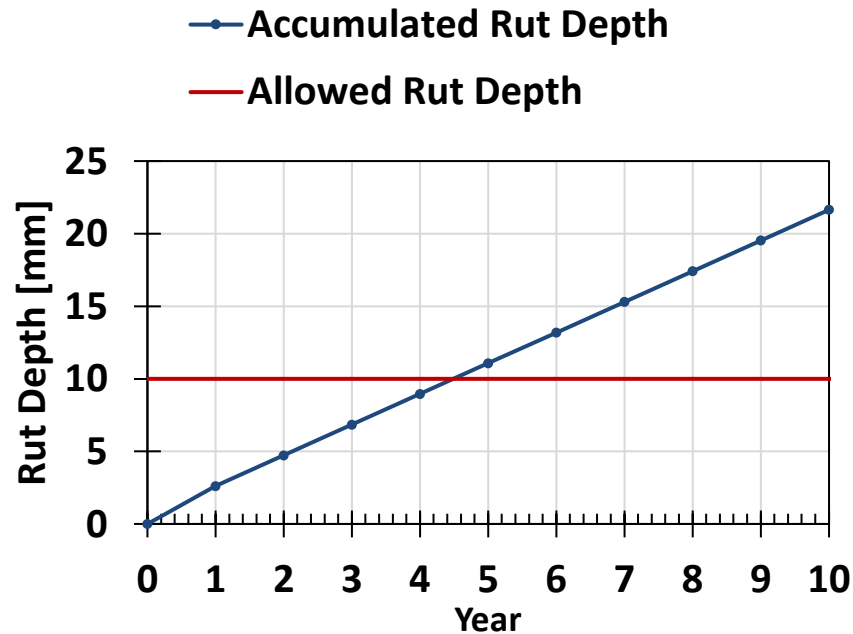
An empirical model based on laboratory testing and calibrated/validated in in-service road tests.

Parameters needed: v , $AADT_L$, Lane width (st. dev.), de-icing, W_p , SST

Two models:

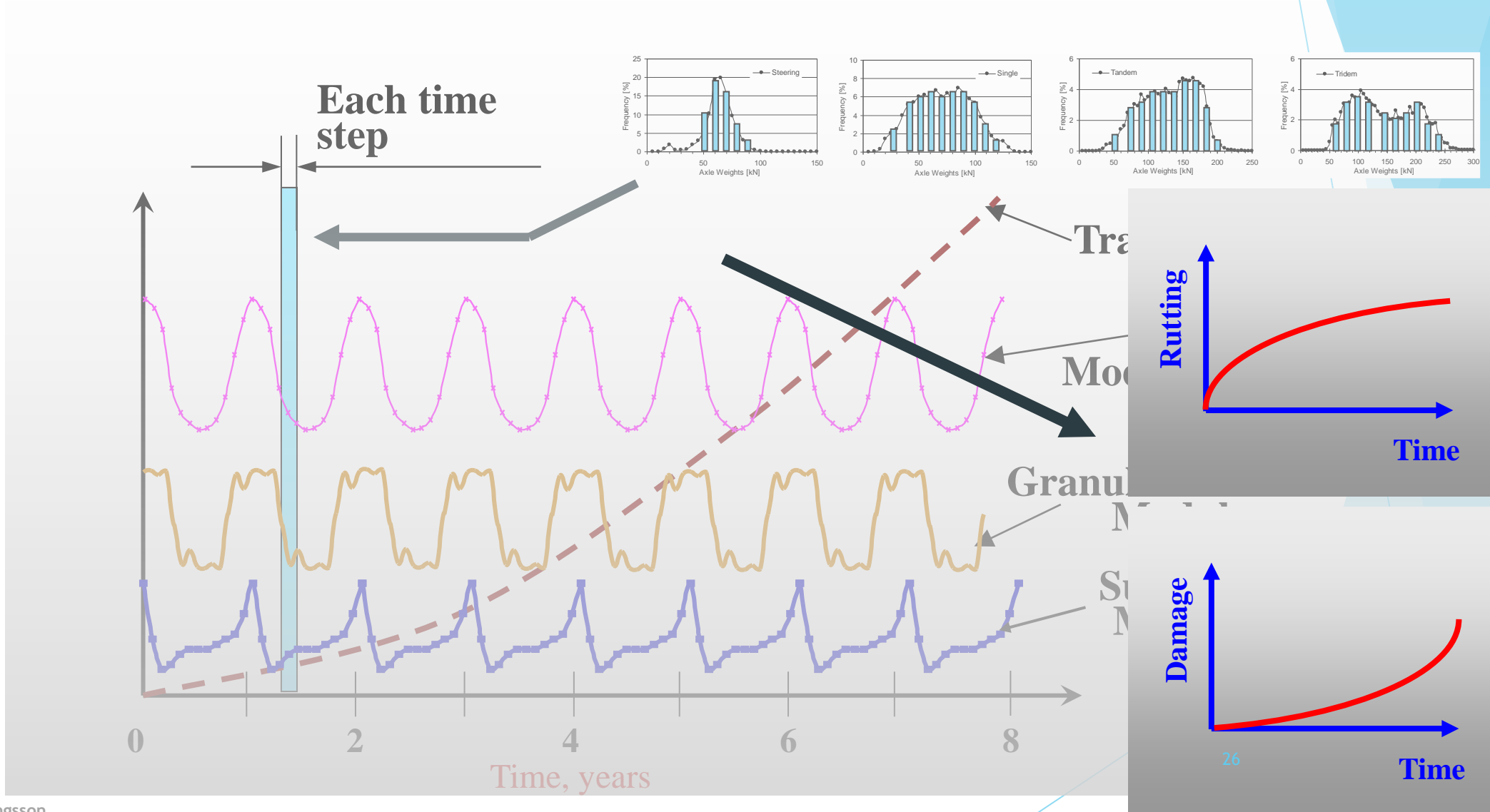
The Nordic abrasion sub-model: A_N , D_{max} , MAS_4

Prall sub-model: A_p



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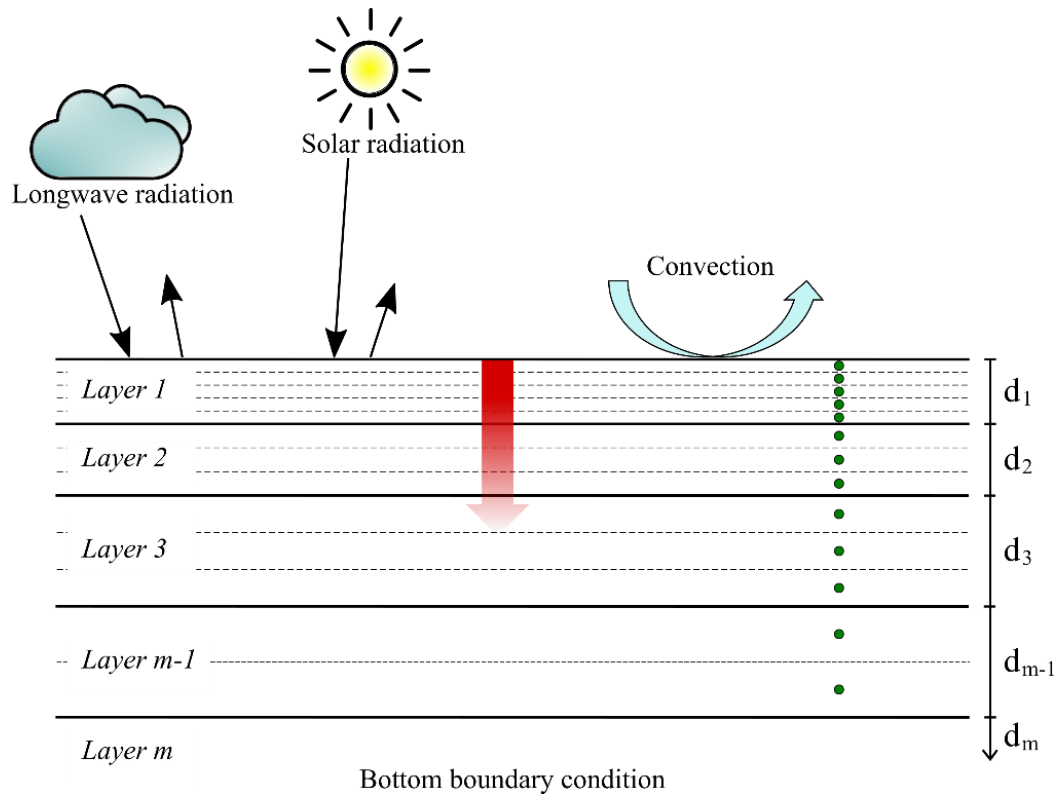
Performance Predictions



Validation (calibration)

- **Climate Predictions**
 - Temperature
- **Response and Performance Predictions**
 - Small scale laboratory testing (RLT tests & ELWT tests)
 - Full scale laboratory testing: APT (HVS)
 - In-service roads
 - LTPP sections
 - Instrumented test sections

Validation - Climate modelling



- External factors considered at the upper boundary condition:

- Air temperature
- Solar shortwave radiation
- Longwave infrared radiation
- Convective heat transfer (wind speed)

- Bottom boundary condition modelled as constant temperature (5m depth)

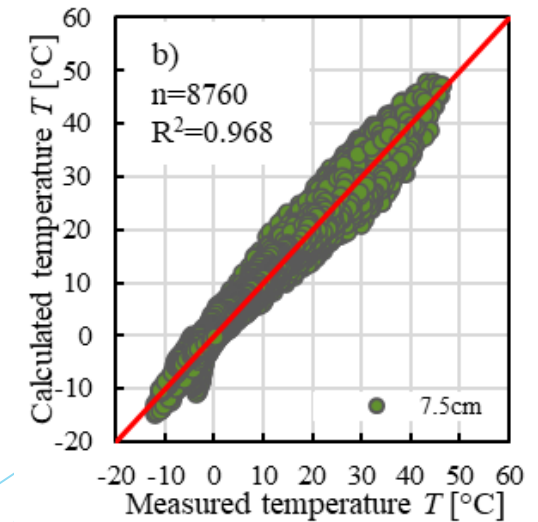
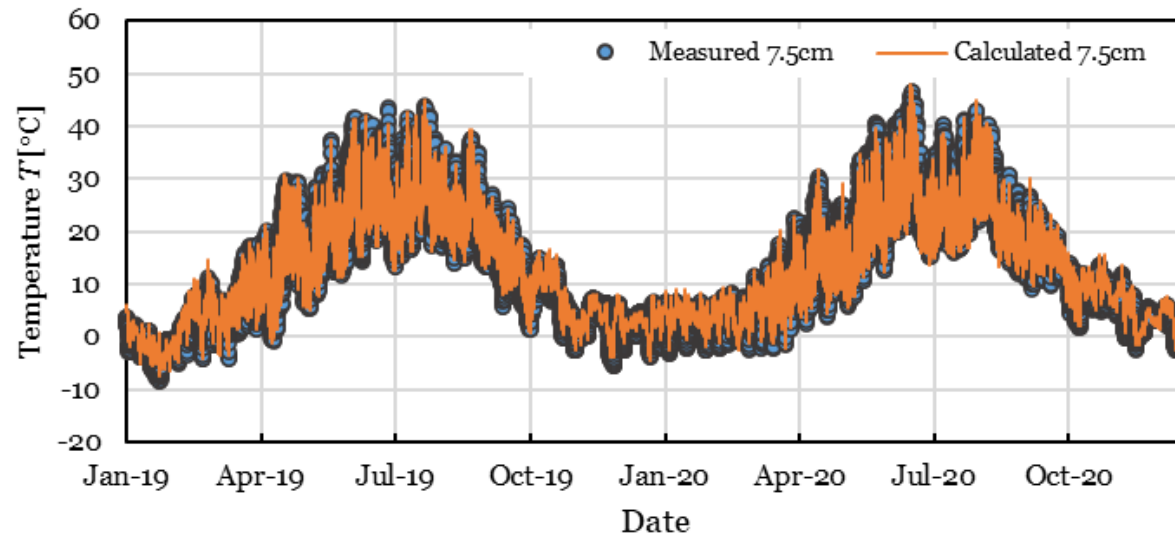
- Temperature distribution in the cross-section given by the 1-D diffusion partial differential equation

$$\rho c_p \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2}$$

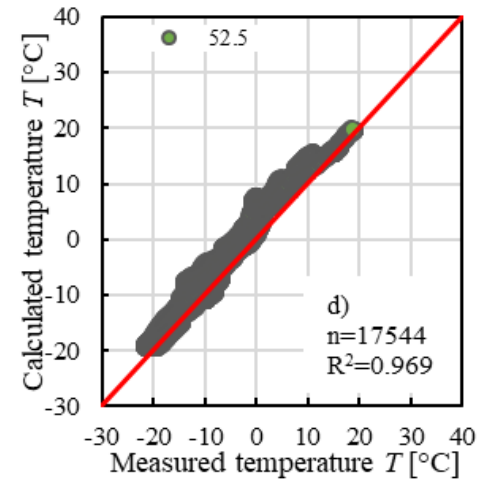
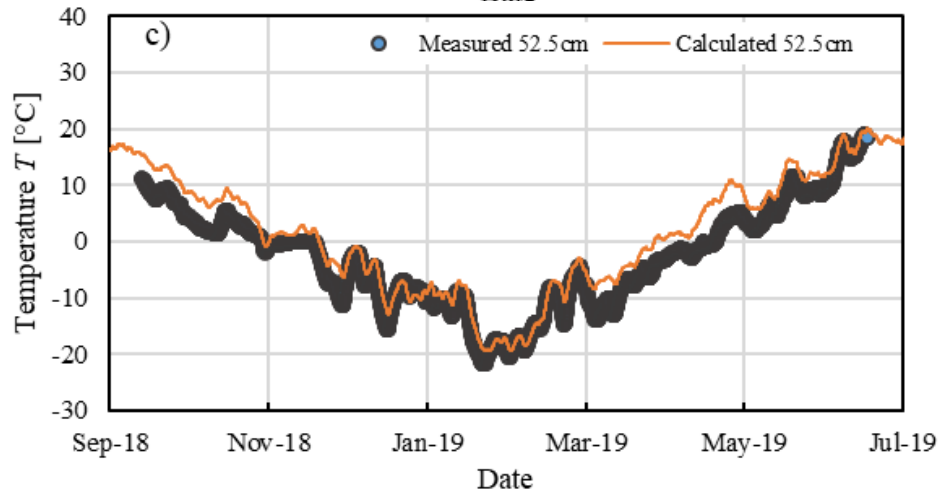
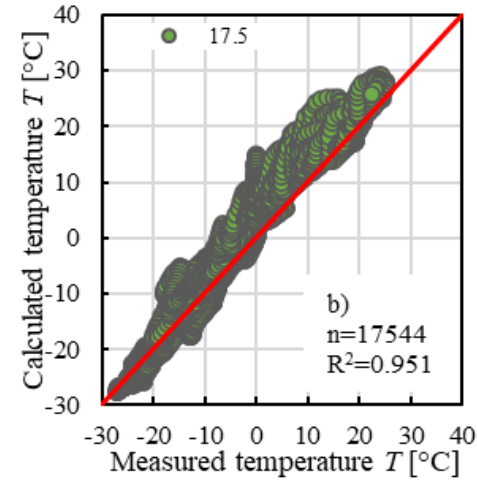
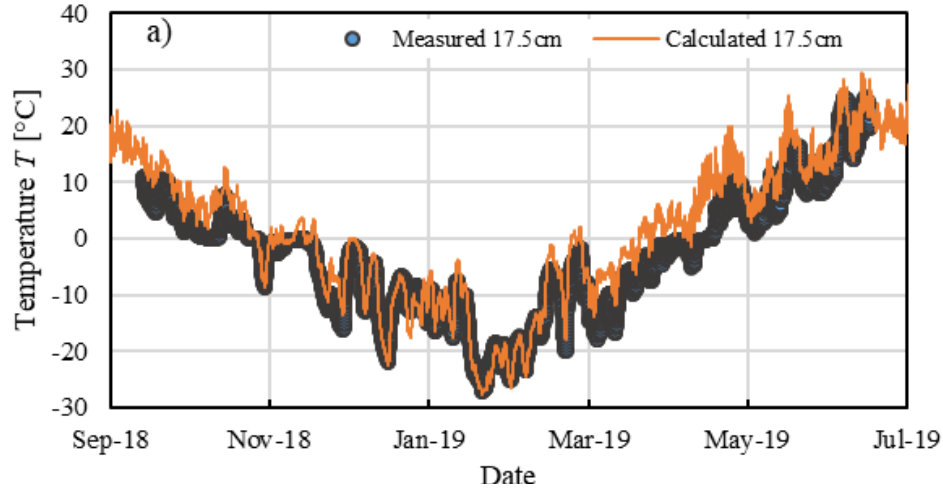
where:
 ρ is the density, kg/m³
 c_p is the heat capacity, J/(kg K)
 k is the conductivity, W/(mK)

- Discretization into finite control volumes (FCV)

Validation - Temperature prediction in AC layers

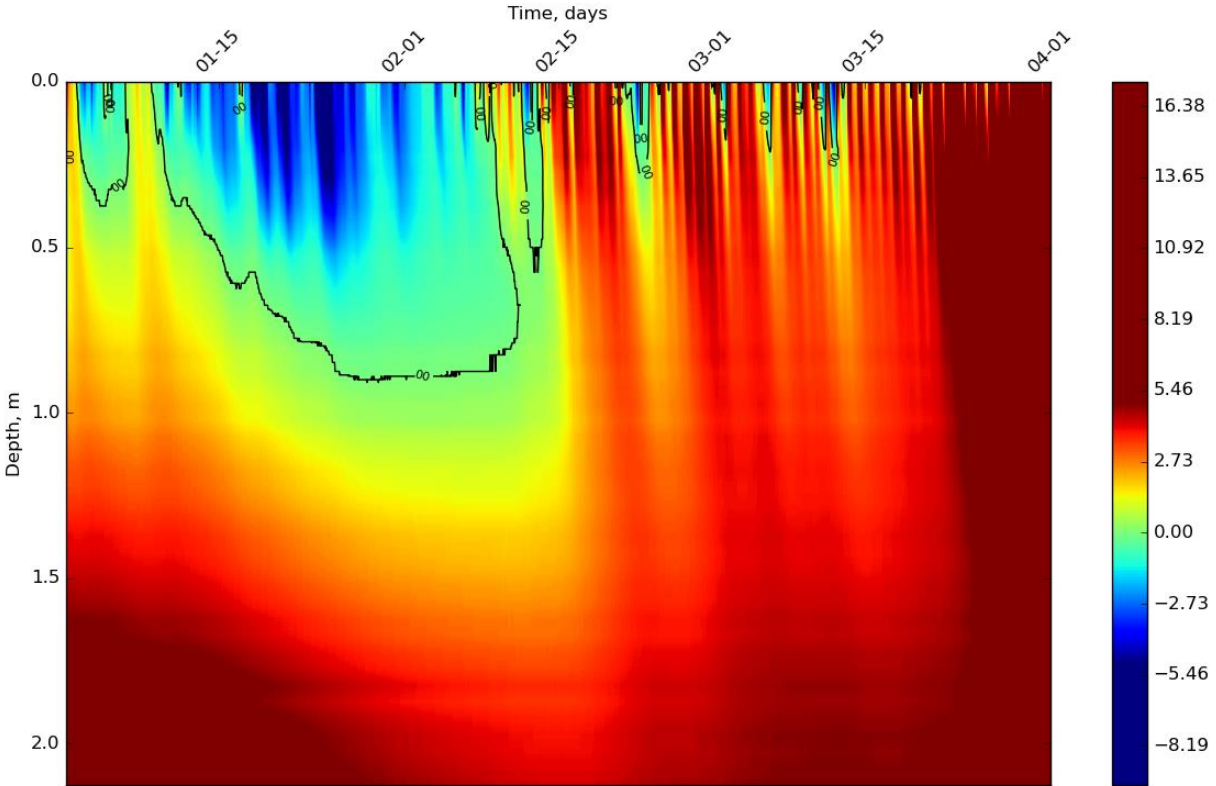


Validation - Temperature predictions in granular layers

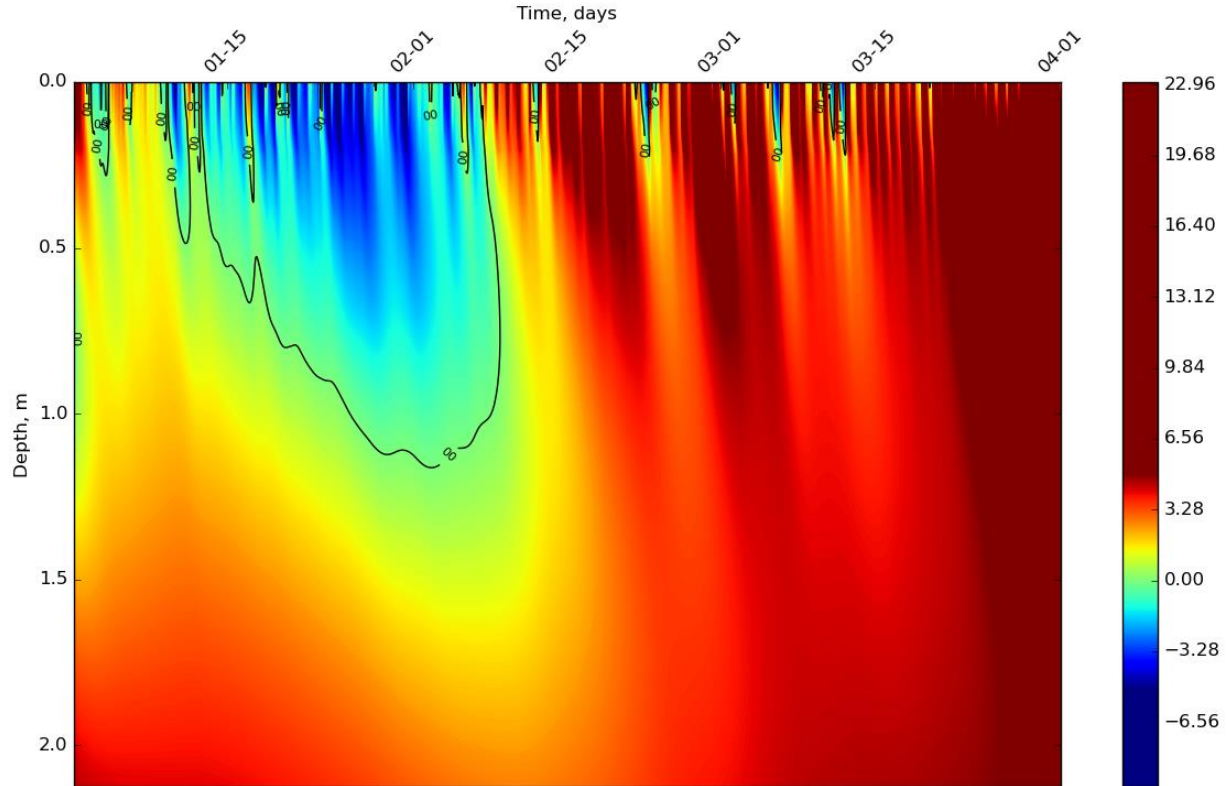


Validation - Frost depth penetrations

Measured

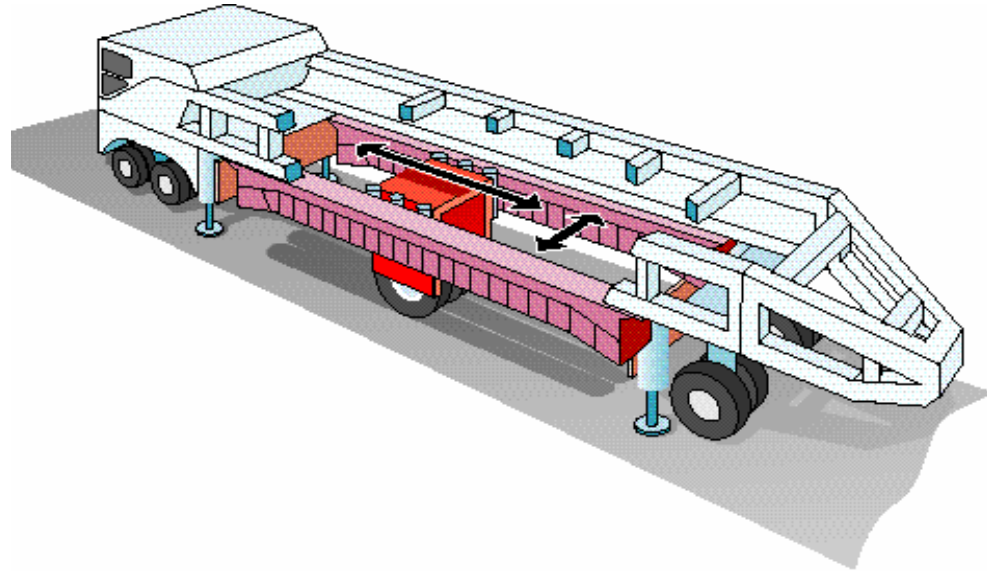


Predicted



Validation: The Heavy Vehicle Simulator (HVS)

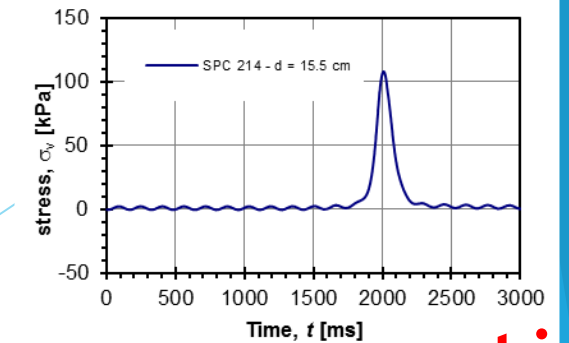
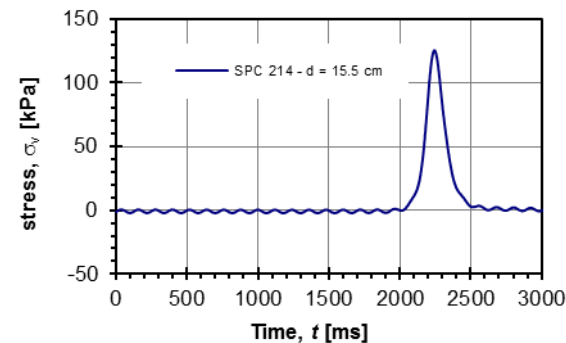
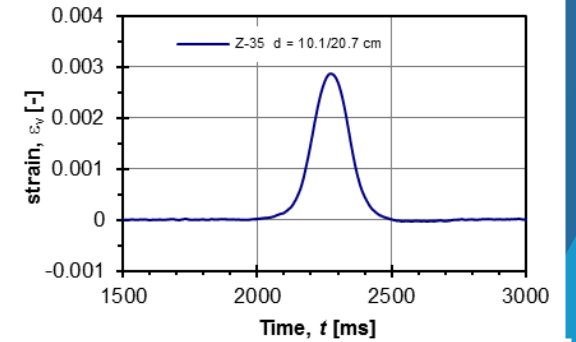
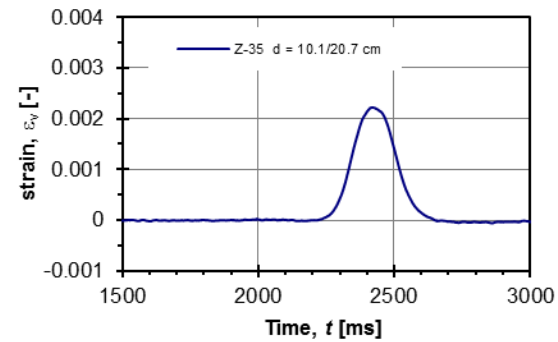
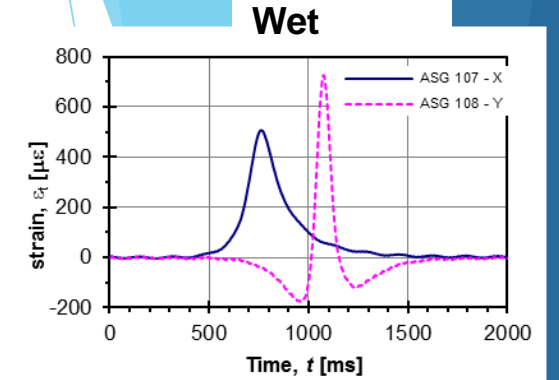
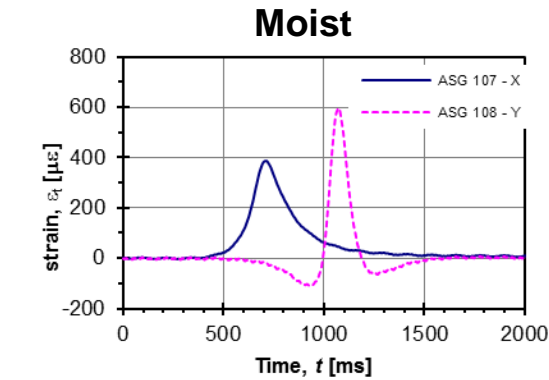
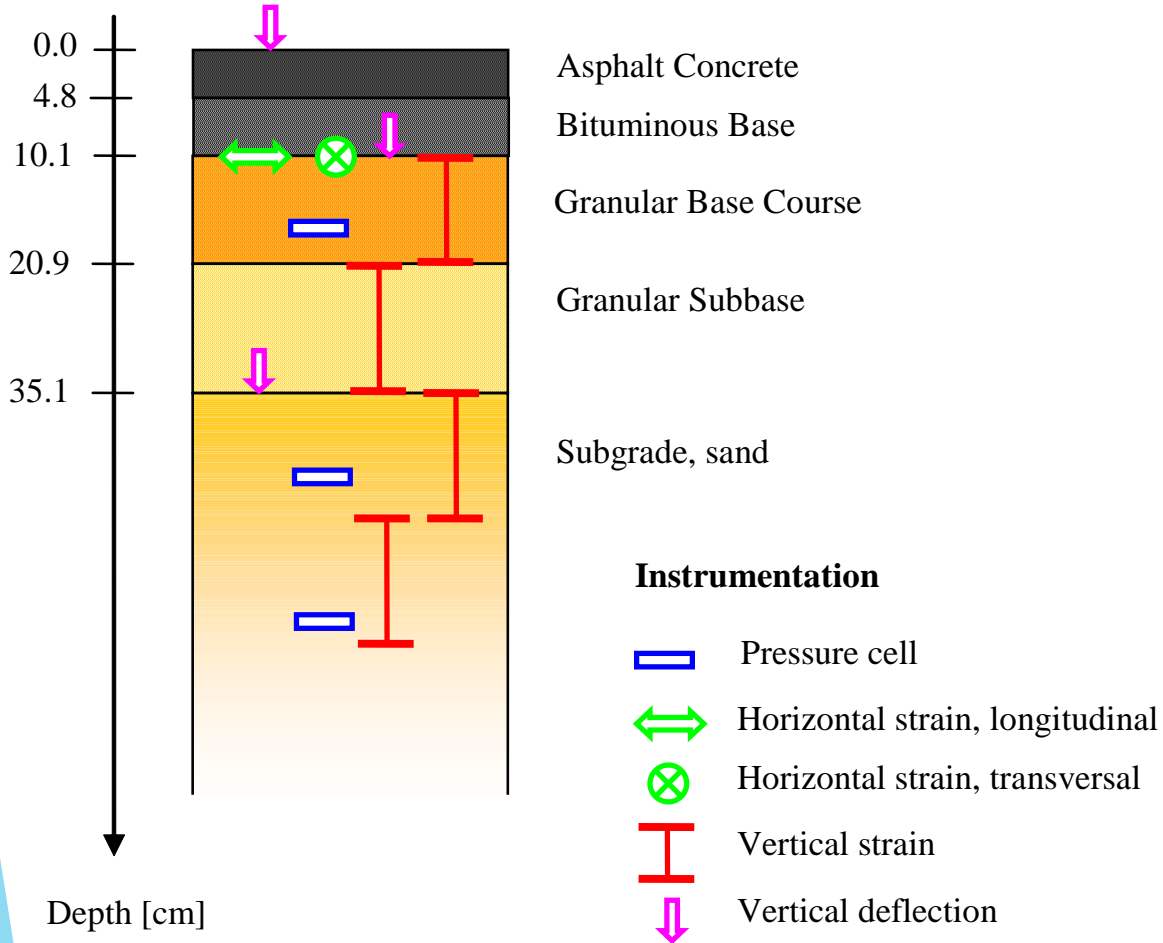
The Heavy Vehicle Simulator (HVS) is a mobile APT test facility.



Validation HVS: Construction of test object



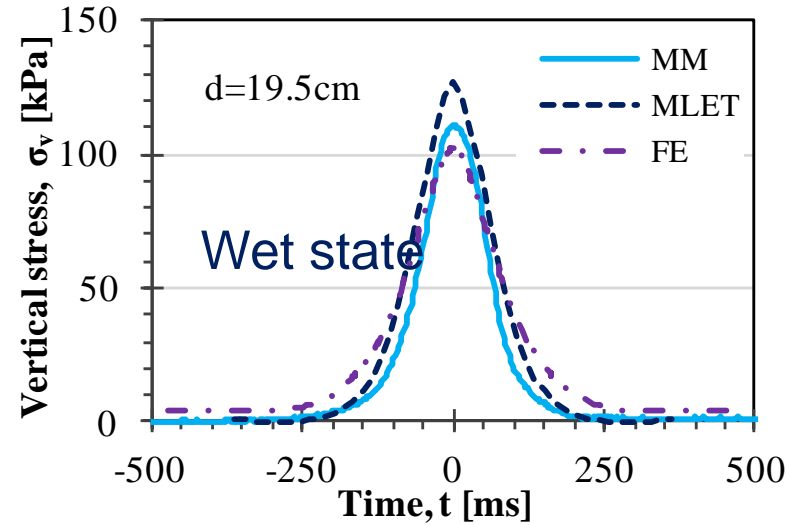
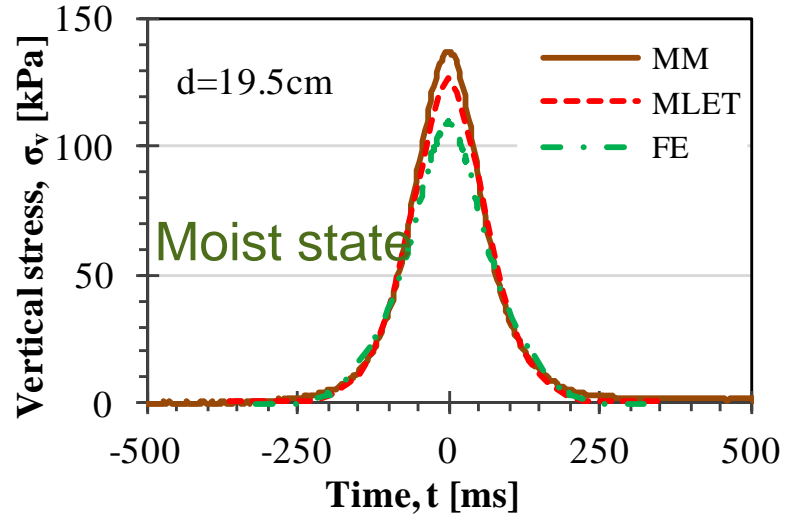
Instrumented test structure: An example



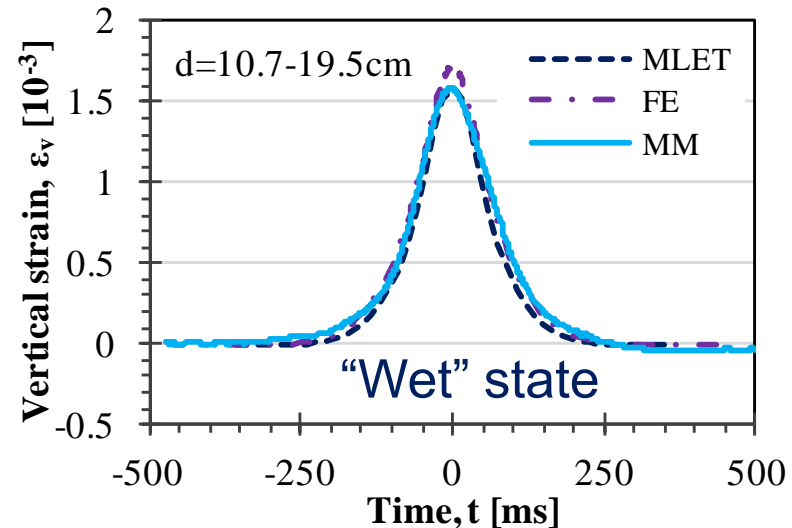
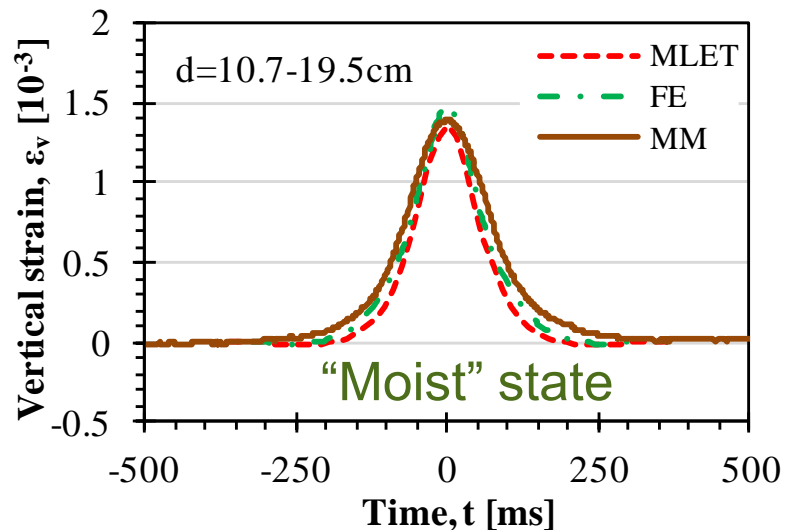
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Response - comp. of measured and predicted values

The response – vertical stress

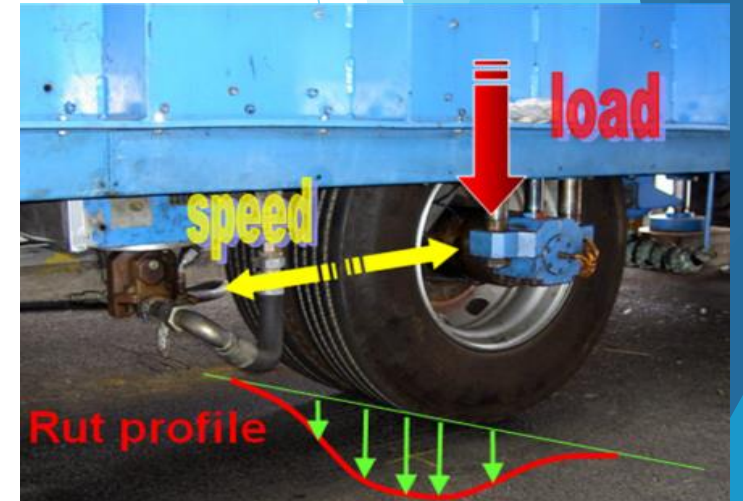
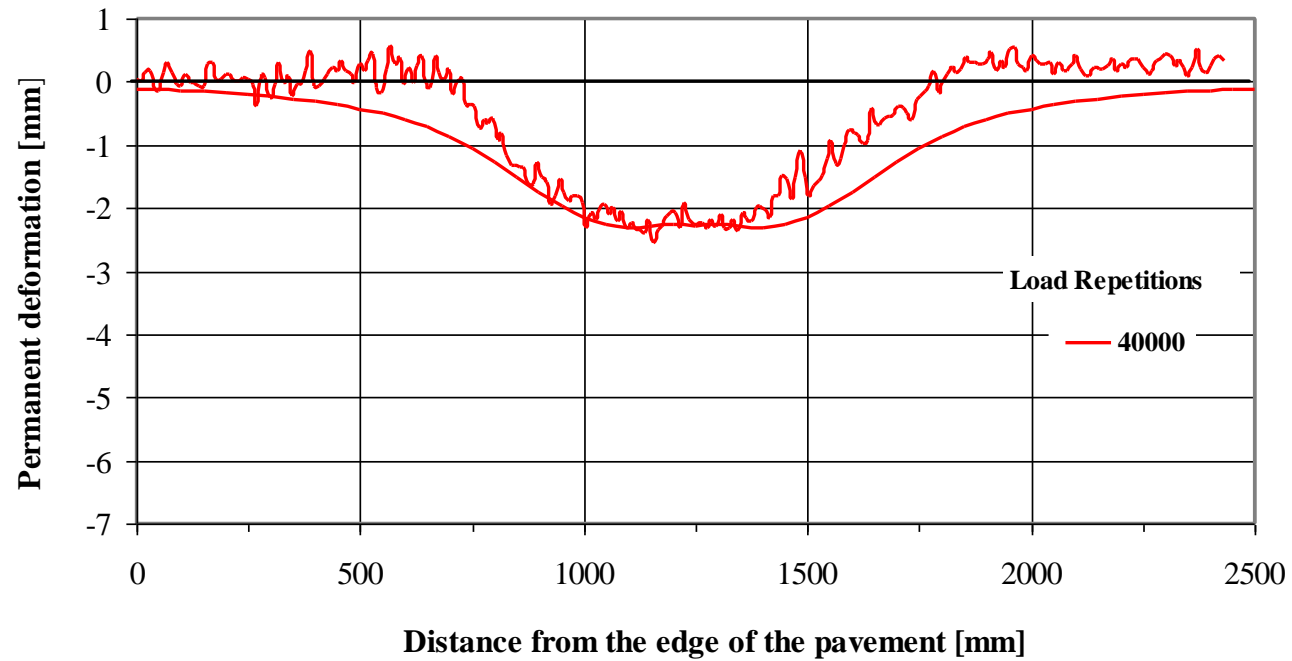


The response – vertical strain

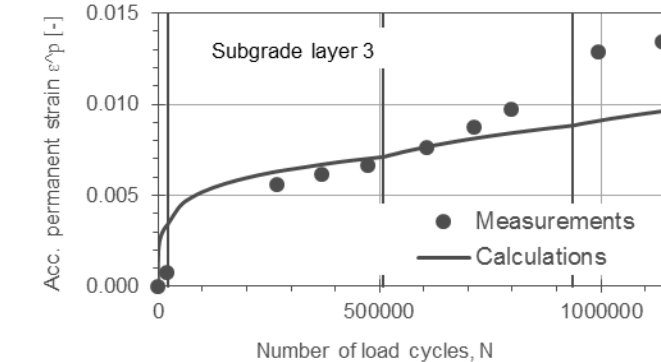
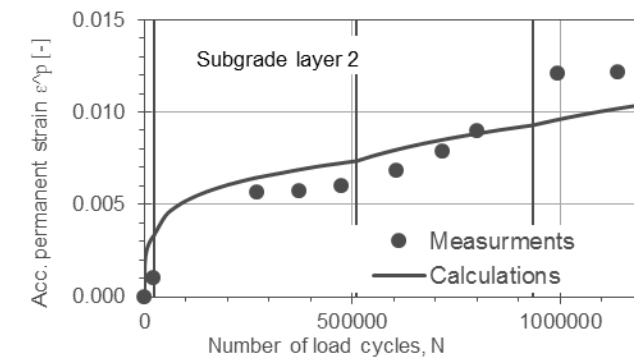
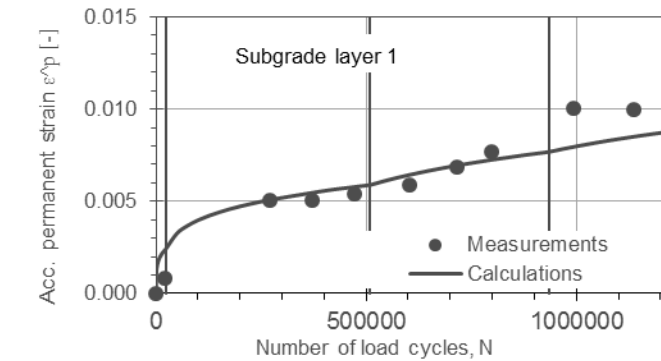
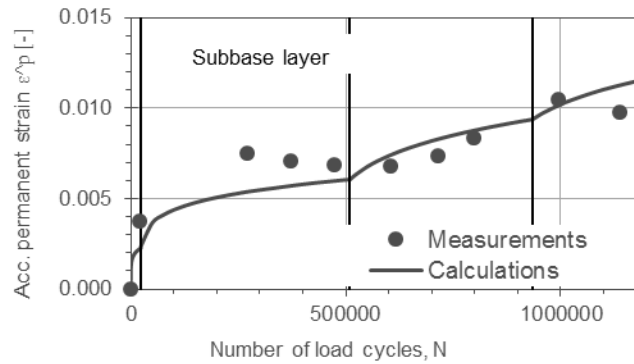
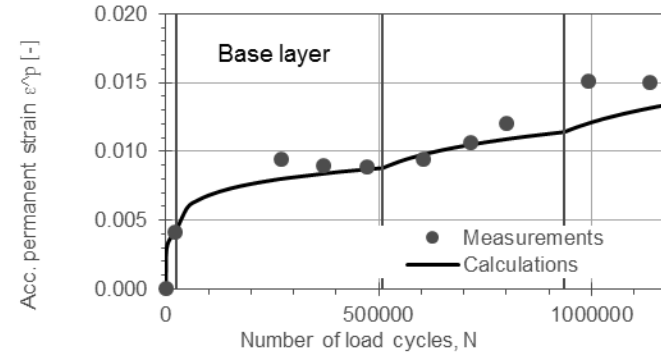
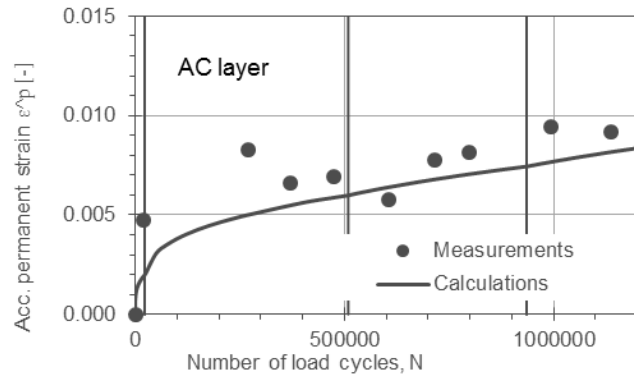
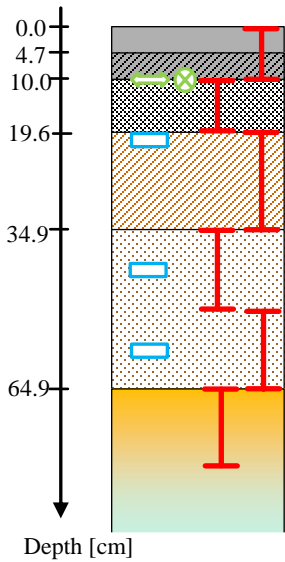


HVS rutting profile

Comparison between measurement and calculation



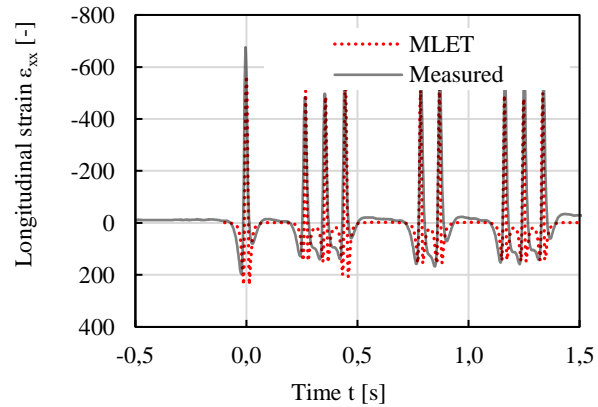
HVS - Validation - vertical permanent strain



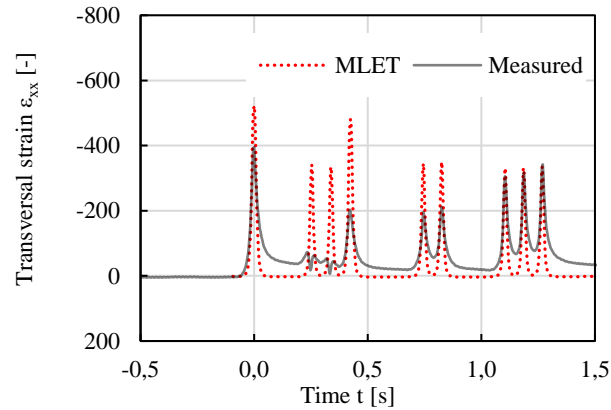
Instrumented in service test sections

MLET - Modelling of response behaviour

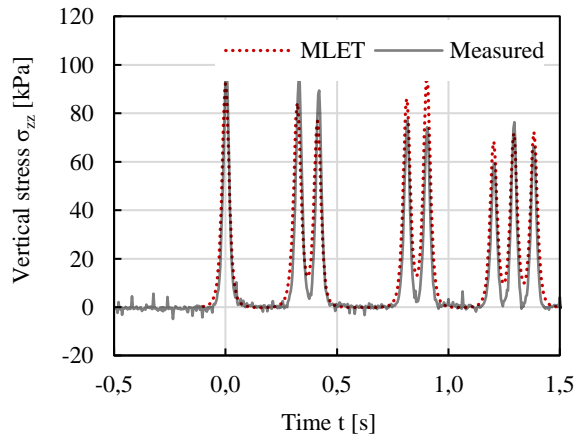
August 2018



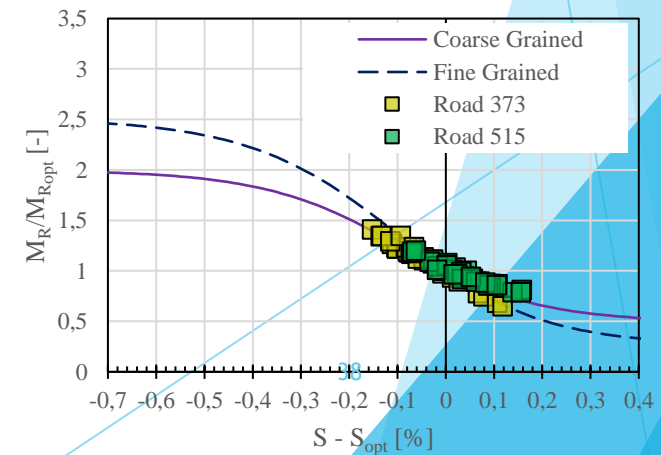
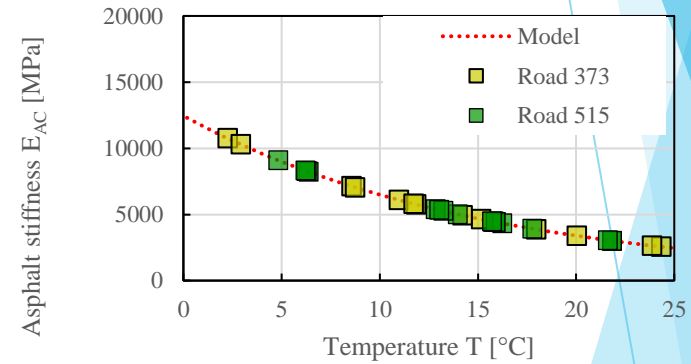
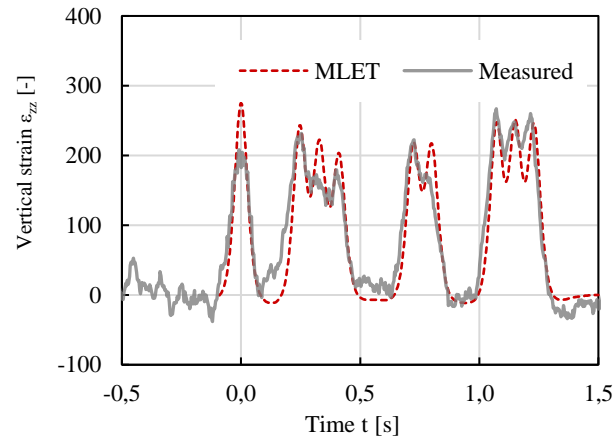
May 2019



June 2019



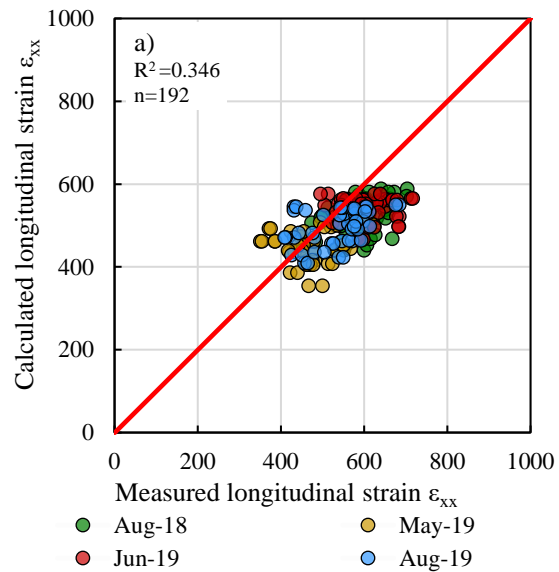
May 2019



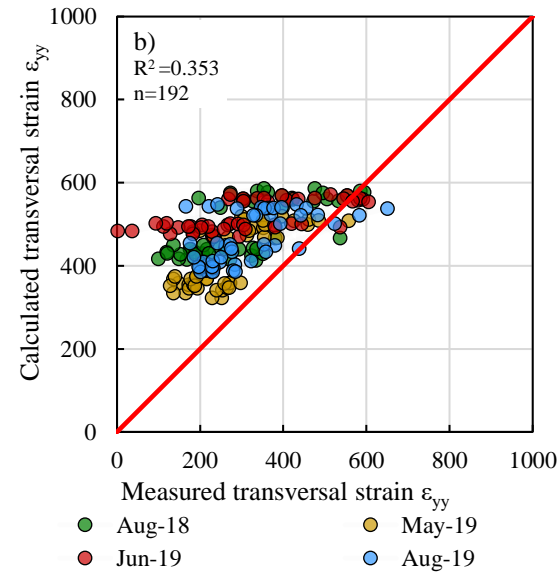
Validation - MLET Response calculations

Two thin pavement structures - peak responses: comparison of measured and predicted values

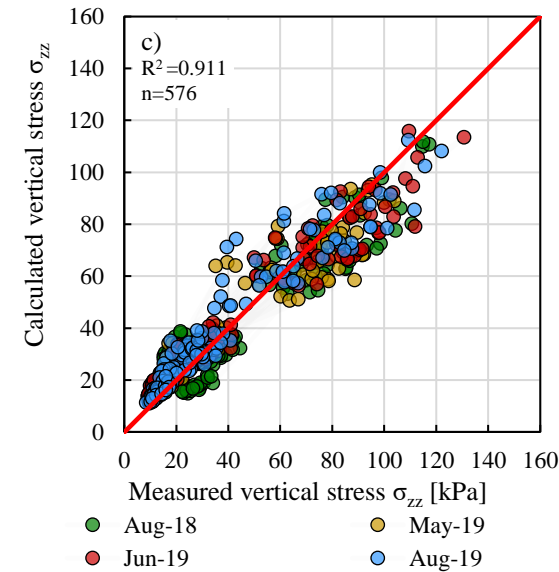
Longitudinal strain



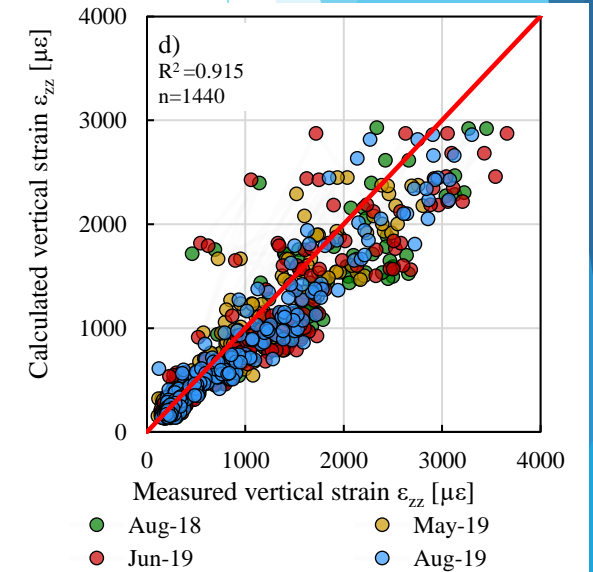
Transversal strain



Vertical stress



Vertical strain



Studded tyre model - calibration

RS rotating in 70 km/h

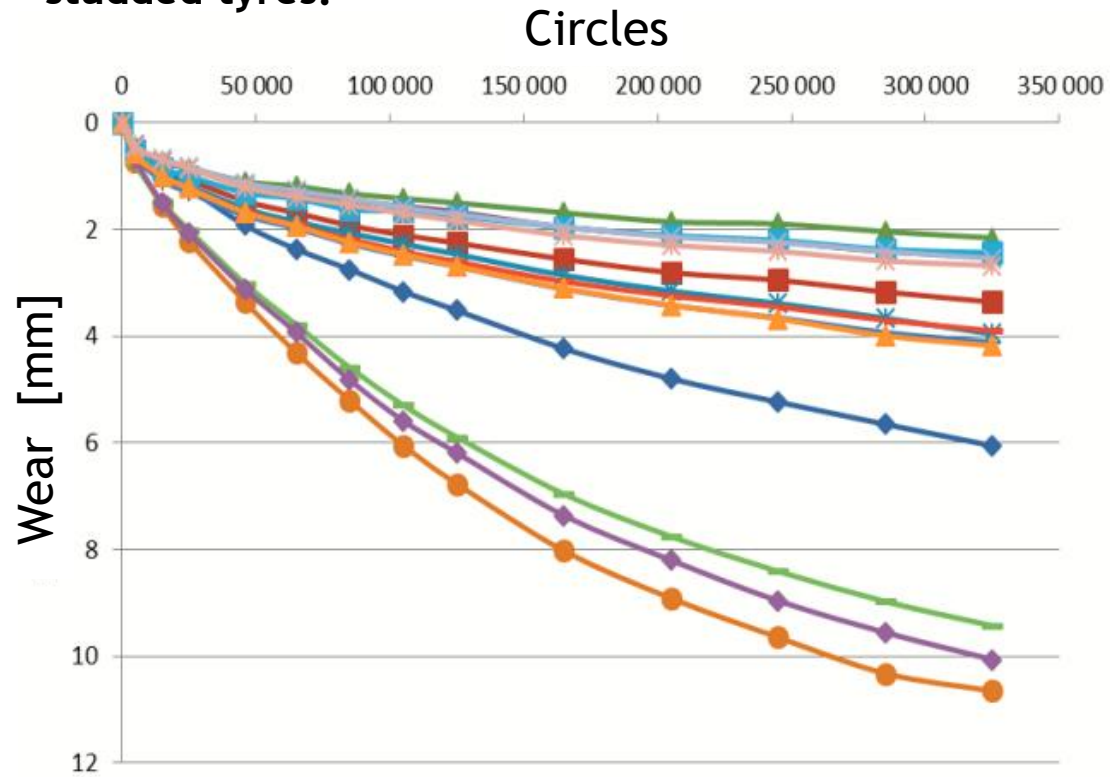


- ▶ Indoor facility:
- ▶ Constant temperature & humidity



Studded tyre wear

Impact of different aggregates on abrasion due to studded tyres.



In service roads - LTPP sections

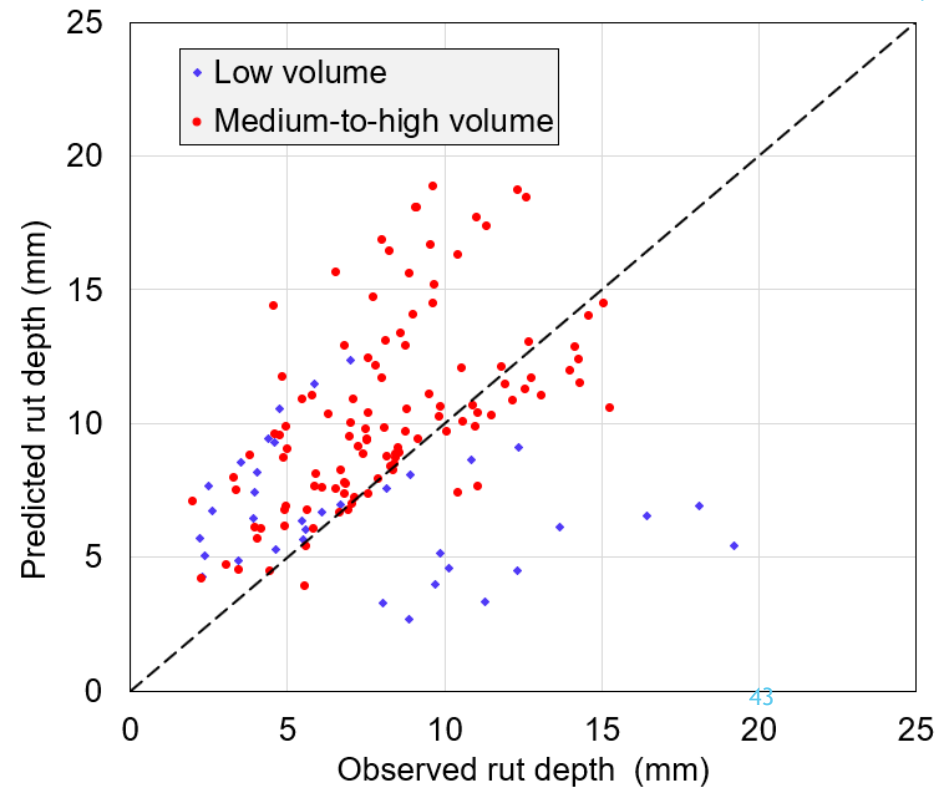
- ▶ 20 unique sections from the Swedish LTPP database
 - ▶ 5 low volume section and 15 medium-to-high volume sections

AADT was used to develop a calibration factor

Category	Road ID	Thickness (mm)			Oppening year traffic (AADT)	Location
		AC	Base	Subbase		
Low volume	C-292-101	85	160	800	787	Uppsala
	C-292-104	35	50	160	787	Uppsala
	U-580-101	80	110	520	400	Västmanland
	U-580-105	80	110	520	400	Västmanland
	W-RV71-101	50	125	500	559	Dalarna
Medium-to-high volume	E-RV34-201	95	120	550	1776	Östergötland
	F-E4-201	150	70	440	5626	Jönköping
	F-RV31-101	50	115	500	2575	Jönköping
	G-126-101	40	160	300	1461	Kronoberg
	G-126-107	40	160	500	1461	Kronoberg
	H-RV34-101	75	125	400	2605	Kalmar
	N-E62-201	180	120	600	6026	Halland
	U-RV56-201	70	150	450	4695	Västmanland
	U-RV56-209	70	75	-	4695	Västmanland
	W-266-101	70	130	500	1897	Dalarna
	W-RV80-101	50	120	500	1403	Dalarna
	X-RV56-101	50	125	400	1053	Gävleborg
	X-RV56-107	50	125	500	1053	Gävleborg
	Y-RV90-101	80	100	900	1748	Västernorrland
	Z-E45-308	130	80	420	2552	Jämtland

Calibration - Original prediction results

- ❑ Original predictions show bias with respect to traffic volume - under-predicting for low volume sections while over-predicting for medium-to-high volume sections
- ❑ Not possible to obtain an optimum calibration equation that captures effectively the various design scenarios



In service roads - LTPP sections - Calibration approach

- ❑ Lack of data from field sections has made it difficult to perform a layer-by-layer model calibration
- ❑ A global calibration factor (k) was introduced to capture the deviation between observed (RD_{obs}) and predicted (RD_{pred}) surface rut depths.
- ❑ Both values include both studded tyre wear and permanent deformation.
- ❑ As traffic volume was observed to have a significant influence on predicted results, the opening annual average daily traffic volume (AADT) was used to derive k .

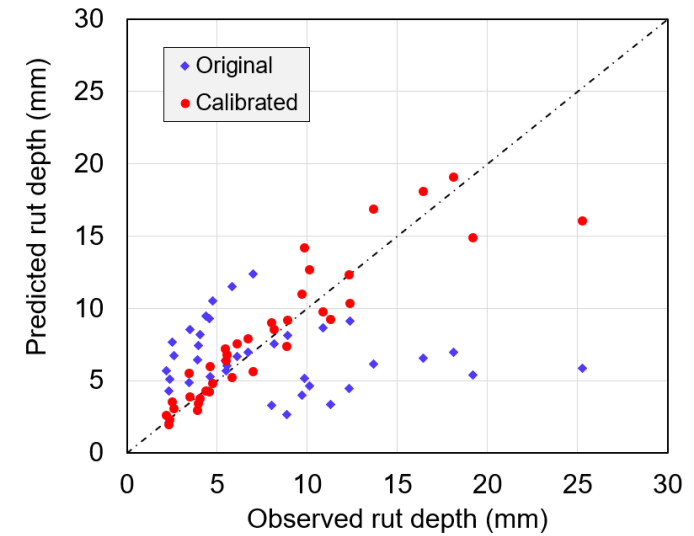
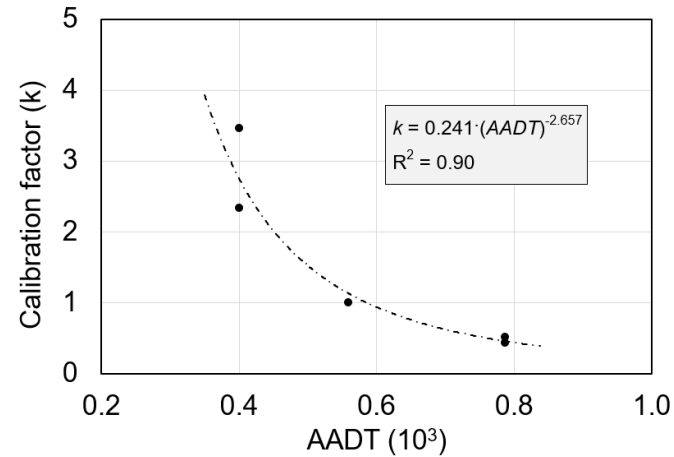
$$k = \frac{RD_{obs}}{RD_{pred}}$$

$$k = a_1 * AADT^{a_2}$$

Calibration - LTPP Field sections

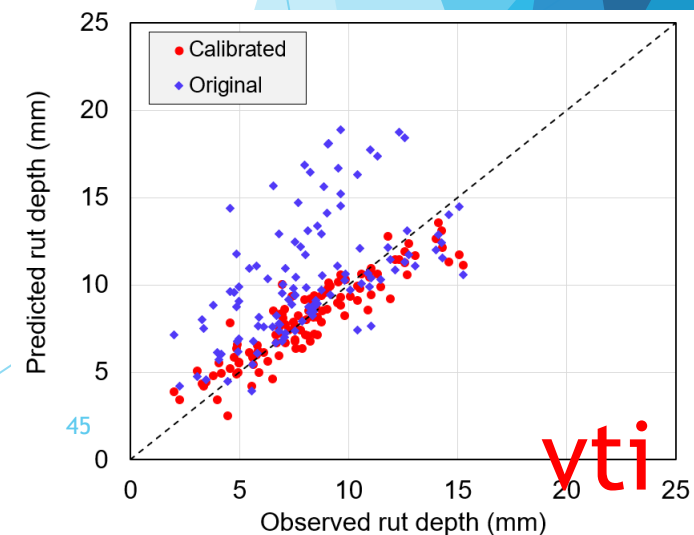
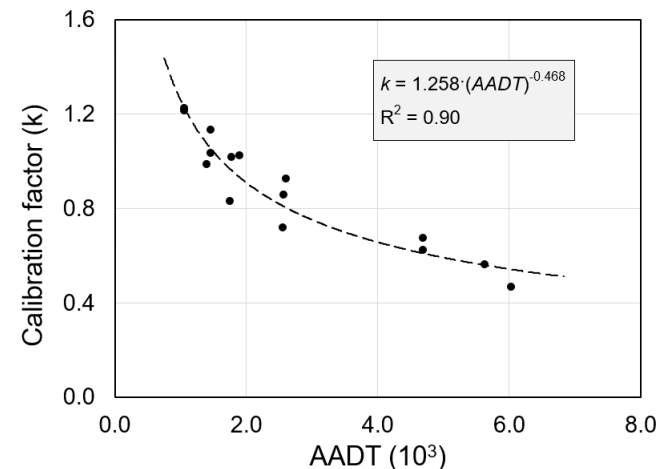
Low volume sections

- ❑ Sections with opening year AADT of 1000 vehicles or less
- ❑ Calibrated model provides acceptable results with R^2 of 0.9
- ❑ Further calibration and validation with more representative sections is required



Medium-to-high volume sections

- ❑ Sections with opening year AADT of more than 1000 vehicles
- ❑ Calibrated model provides acceptable results with R^2 of 0.9
- ❑ Model validation is required to evaluate the capability of the calibrated model



Instrumented/LTTP in-service roads

Next steps

- ▶ Two new test sites:
 - ▶ Upgrade of test site E18
 - ▶ New test site E16 Amsberg

Test site E18

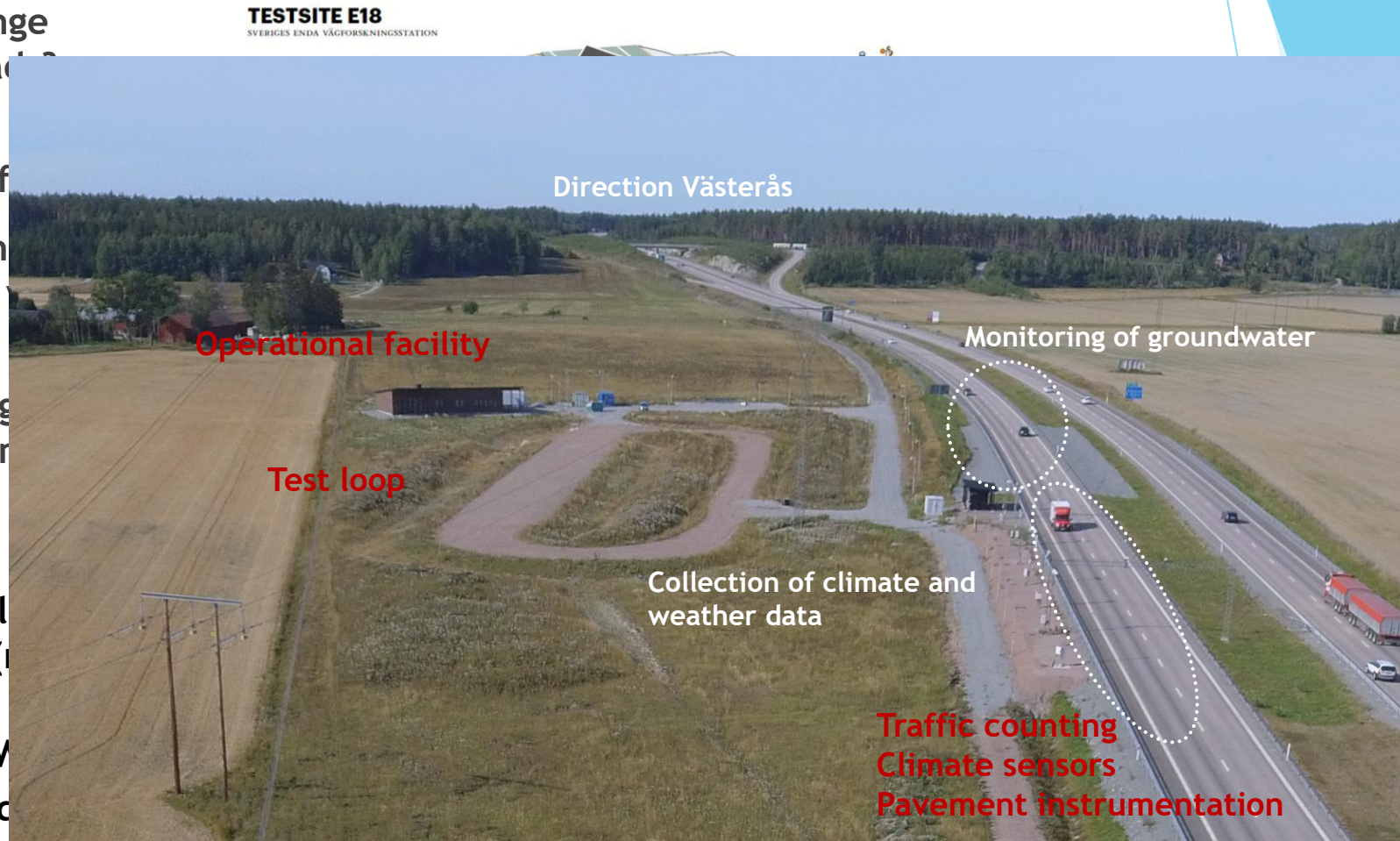
An environmental and road research site on Motorway E18 established in 2010.

- ▶ How are climate change affecting Swedish roads?
- ▶ How is groundwater contaminated by traffic?
- ▶ How much salting is used in Sweden and how can we reduce its impact?
- ▶ How effective is ploughing and salting during the winter months?

The research program will include:

- pavement mechanics (road performance).

- traffic monitoring (V)
- sensor monitoring (c)
- a new testing loop



Test site E16 Amsberg

- ▶ A new research station **Test site E16 Amsberg** is under construction.
- ▶ The objective is to remotely monitor climate, traffic and pavement performance for better understanding their interactions.
- ▶ The monitoring programme will include:
 - ▶ **Climate**
 - ▶ Weather station (Air temperature, wind speed, precipitation and solar radiation)
 - ▶ Temp in AC layers, Frost rod, moisture rod, suction, groundwater table.
 - ▶ **Traffic**
 - ▶ Video camera, WIM system, Inductive loops.
 - ▶ **Pavement Performance**
 - ▶ ASG - Tensile strain (longitudinal & transversal),
 - ▶ SPC - Soil pressure cells
 - ▶ Emu coils - vertical strain
 - ▶ Accelerometers & Geophones (surface deflections).



Material databank

- ▶ A Material databank is under development.
- ▶ Includes:
 - ▶ Common types of AC materials:
 - ▶ Surface course
 - ▶ Binder course
 - ▶ Road base
 - ▶ Unbound base course
 - ▶ Crushed rock aggregate
 - ▶ Open graded material
 - ▶ etc.
 - ▶ Subbase
 - ▶ Subgrade

The screenshot shows the ERAPave software interface. The main window is titled 'Structure' and contains a table of pavement layer types and thicknesses. The table has columns for Layer, Material, and Thickness (mm). The layers are:

Layer	Material	Thickness (mm)
1	ABT11 70/100_modified	40
2	ABb16 50/70_modified	50
3	AG22 160/220_modified	50
4	GW-CR (4-6% fines)	80
5	GW-CR (4-6% fines)	420
6	4e - Lera	#####

Below the table, there are radio buttons for 'Drainage class of the pavement structure' with options: Well, Medium (selected), and Poor. There are also buttons for 'Add layer', 'Remove layer', 'Move up', 'Change material', and 'Save layer data to local database'. To the right of the table is a cross-section diagram of the pavement structure with a legend for the layers: Layer 1 40 mm (black), Layer 2 50 mm (dark grey), Layer 3 50 mm (medium grey), Layer 4 80 mm (light grey), and Layer 5 420 mm (orange). The bottom of the interface has a 'Run' button and a 'Cancel' button, and a 'RESULTS' section with 'Results in Excel' and 'Generate Report' buttons.

Summary

- ▶ ERAPave PP is a new M-E based software for structural design of flexible pavements.
- ▶ The software is still under development (Version 0.93 available).

Some further developments:

- The user-interface needs further improvements. A user manual will be published.
- A material databank is under development.
- The climate (water balance - moisture) needs to be better included in the design (performance calculations).

and

- Further validation of performance predictions is needed.
 - Smoothness (IRI), Low temperature cracking
- Performance based laboratory/field testing
- Update of the studded tyre (abrasion) model
- Rehabilitation (Design of overlays)
- Surface profile parameters

Thank you for your attention!

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abubeker.ahmed@vti.se